

# Three Principles of Designing Base-Station Antennas

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**Abstract**—Three principles of designing base-station antennas are proposed: wide band impedance match, stable radiation patterns in wide frequency band and high cross polarization ratio in wide angle range.

**Keywords**—Base-station antenna; wideband impedance match; stable radiation patterns; cross polarization ratio

## I. INTRODUCTION

Recently, different mobile communication systems have been designated with different frequency bands. In China, the 2G systems such as GSM, CDMA operate in 1710-1920MHz band, the 3G systems such as WCDMA, TD-SCDMA and CDMA2000 operate in 1880-2170 MHz band and the 4G LTE systems operate in 2300-2400 MHz and 2570-2690 MHz bands. Therefore, the base-station antennas simultaneously cover 1710-2690 MHz band are necessary for modern mobile communication systems. The base-station antennas should achieve not only wideband impedance match ( $VSWR < 1.5$ ), but also stable 3-dB beamwidth with  $65 \pm 5^\circ$  for horizontal plane. For  $\pm 45^\circ$  dual polarized base-station antennas, cross polarization ratio (XPD) also should be higher than 20 dB at broadside and 10 dB at  $\pm 60^\circ$ .

Many methods have been proposed to broaden the impedance wideband of dipoles. Log-periodic antennas or equiangular spiral antennas can achieve wideband impedance matching, but they are bulky in their structures [1]. The patch antennas with a meandering probe [2], an L-probe [3], or an U-slot patch [4] can increase impedance bandwidth, but the radiation patterns vary substantially over the operation frequencies. In order to achieve wideband beamwidth, a wideband antenna called magnetoelectric dipole with 43.8% impedance bandwidth ( $SWR < 1.5$ ) was proposed [5] recently. By combining a planar electric dipole and shorted patch antenna, stable radiation pattern with 3-dB beamwidth  $73 \pm 6$  degree for E-plane and  $76 \pm 4$  degree for H-plane [6] in desired band was achieved. This work has attracted wide attentions and in depth studies [7]. Only a few studies in literature are concerned with improving the XPD within  $\pm 60^\circ$  of the main lobe at the horizontal plane. In [8], the antenna has high XPD at the center frequency. In [9], the XPD of the antenna at the boresight is given. Previous studies about XPD [10]-[12] have not concentrated on how to improve XPD for  $\pm 45^\circ$  dual-polarized base station antennas. In [13], XPD of a vertical-horizontal dual-polarized antenna was studied. However, XPD of a  $\pm 45^\circ$  dual-polarized antenna is different from that of

vertical-horizontal dual-polarized antenna, in terms of the measuring method of antennas. Two parasitic elements were added to reduce the cross-polarization of a patch antenna [14]. A  $45^\circ$  slant-polarized antenna was proposed in [15]. It can be seen from the measuring method that, for  $\pm 45^\circ$  dual-polarized antenna, even if all the dipoles are in ideal case, it is still hard to achieved high XPD in all polar angles. Currently, engineers working in antenna companies adjust the antenna structures to improve XPD by a trial and error basis, because there are few theories for improving XPD.

In this paper, three principles of designing base-station antennas are proposed: wide band impedance matching, stable radiation patterns in wide frequency band and high cross polarization ratio in wide angle range. Several base-station antennas with good performance are design, fabricated, and measured.

## II. PRINCIPLE OF WIDEBAND IMPEDANCE MATCHING

Similar to a resonator, a dipole always has many resonant modes whose frequencies are not close to each other originally. Also similar to a multi-mode filter, If the resonant modes can get close to each other, wideband impedance match could be reached as shown in Fig.1. For example, a dipole as shown in Fig.2(a) can resonate in half wavelength and one wavelength, its input impedance is shown in Fig.3. It can be found that the dipole has one resonant mode at 2.3 GHz and another resonant mode at 4.8 GHz. While the dipole is loaded a stub as shown in Fig.2(b), the two resonate modes are close to 2.3 GHz as shown in Fig.4, therefore, wideband impedance match is achieved as shown in Fig.5.

## III. PRINCIPLE OF STABLE RADIATION PATTERNS

Fig.6 shows two parallel dipoles with the same phase over a big reflector. Following the image method, the two dipoles can be equivalent to the four dipoles as shown in Fig.7. The principle of broadband radiation patterns is shown in table I. As increase of frequency, the beamwidth of a dipole becomes narrow in the E-plane, while the beamwidth of an out-phase binary array (i.e. a point source and a reflector) becomes wide. So a stable beamwidth of the total radiation pattern in the E-plane is achieved. For H-plane, the beamwidth of an in-phase binary becomes narrow as increase of frequency, while the beamwidth of an out-phase binary array becomes wide. Therefore, a stable H-plane of total radiation pattern is also obtained. In a word, stable beamwidths at E- and H-planes are obtained in wide frequency band.

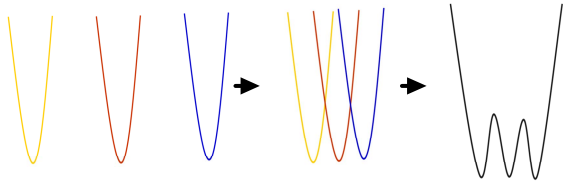


Fig. 1. Principle of wideband impedance matching



Fig. 2. A dipole (a) not loaded a stub (b) loaded a stub

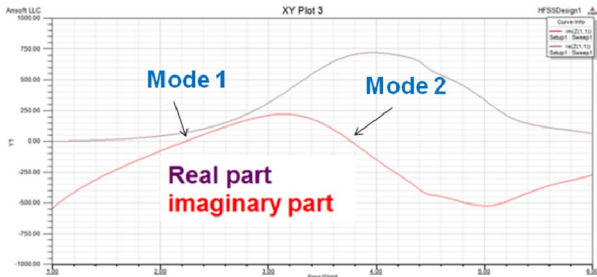


Fig. 3. Input impedance of a dipole

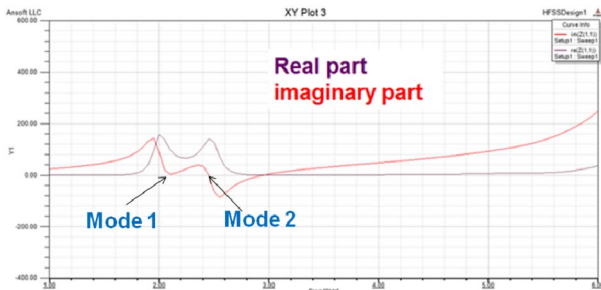


Fig. 4. Input impedance of a dipole loaded a stub

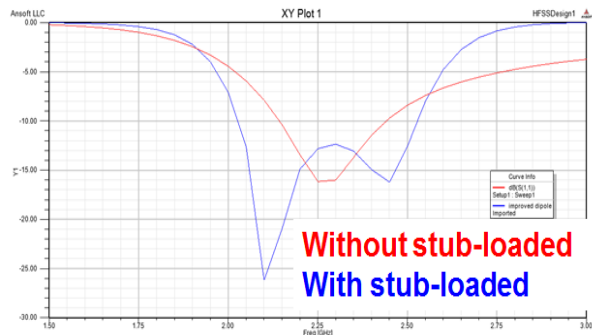


Fig. 5. Reflection parameter of the dipoles

#### IV. PRINCIPLE OF HIGH XPD IN WIDE ANGLE RANGE

For 4G basestation antennas, cross polarization ratio (XPD) must higher than 20 dB at broadside and 10 dB at  $\pm 60^\circ$ . A simple  $\pm 45^\circ$  dual polarized basestation antenna cannot satisfy the requirement. Fig. 8. presents a schematic diagram of

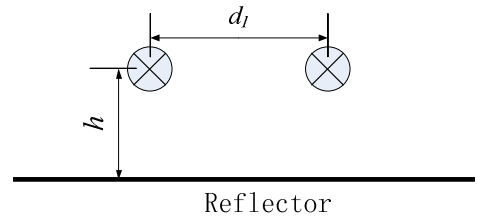


Fig. 6. Two dipole with the same phase over the big reflector.

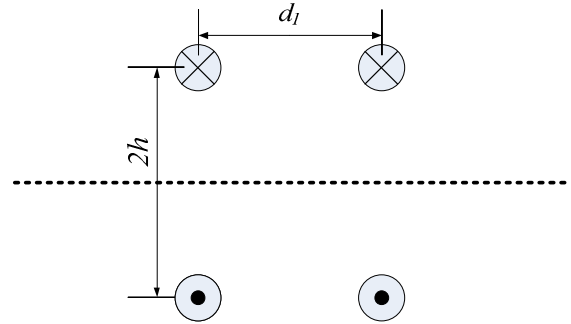


Fig. 7. Analysis of Fig. 6 by image method

TABLE 1. PRINCIPLE OF STABLE RADIATION PATTERNS

$-0.8f_0$ $-f_0$ $-1.2f_0$	Radiation pattern of a dipole	Radiation pattern of an in-phase binary array	Radiation pattern of a point source and a reflector	Total radiation pattern
		$\times$	$\times$	$=$
		$\times$	$\times$	$=$

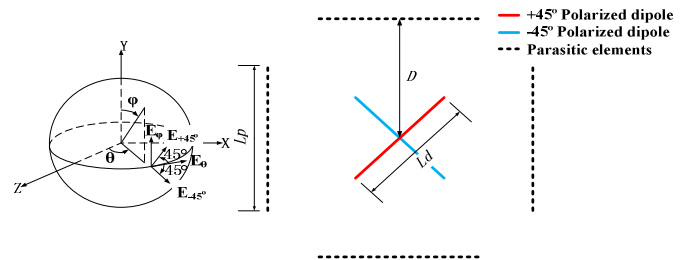


Fig. 8. Schematic of the proposed  $\pm 45^\circ$  dual-polarized antenna with four parasitic elements in a square contour.

TABLE I  
EFFECT OF PARASITIC ELEMENTS ON XPDs

	$0^\circ$	$+60^\circ$	$-60^\circ$
Without parasitic elements	$+\infty$	9.54	9.54
With parasitic elements	$+\infty$	20.0	20.0

the proposed dual-polarized antenna with four parasitic elements in a square contour. Every  $\pm 45^\circ$  dual-polarized antenna can be simplified approximately to a  $+45^\circ$  polarized dipole (red thick solid line) and a  $-45^\circ$  polarized dipole (blue thick solid line). Four parasitic elements (black dashed line) were placed on the four sides of a square contour. The effects of the parasitic elements on XPD are shown in Table I. It can be seen that after the addition of parasitic element, the XPD are improved at  $\pm 60^\circ$  and still large at broadside.

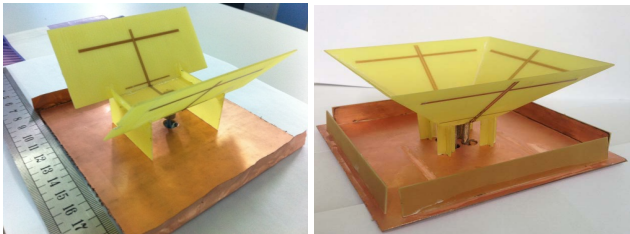


Fig.9. Base-station antenna in [16]. Fig. 10. Base-station antenna in [17].

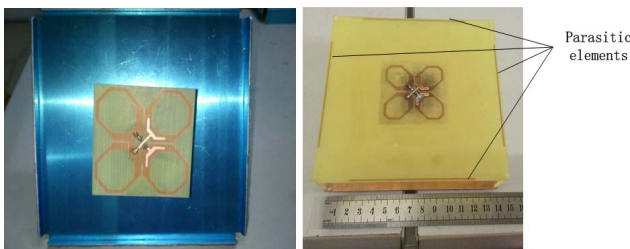


Fig.11. Base-station antenna in [18]. Fig.12. Base-station antenna in [19].

## V. CONCLUSION

Three principles have been proposed to design 4G base-station antennas. According to the principles, a series of antennas with high performance have been designed, fabricated and measured as shown in Fig.9-Fig. 12 [16]-[19].

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