

# Modified Pseudo Orthogonal M-sequence Sets for Synchronous Optical-CDMA

Yusuke Kozawa<sup>1</sup> and Hiromasa Habuchi<sup>2</sup>

<sup>1,2</sup>College of Engineering, Ibaraki University

4-12-1 Nakanarusawa Hitachi, Ibaraki 316-8511, Japan

E-mail : <sup>1</sup>07nm707r@hcs.ibaraki.ac.jp, <sup>2</sup>habuchi@mx.ibaraki.ac.jp

**Abstract:** In this paper, to increase normalized throughput of the optical code-division multiple-access (CDMA) system, optical-CDMA systems with multi-pulse pulse position modulation (MPPM) using the modified pseudo orthogonal M-sequence sets is proposed. The throughput performance and bit error rate (BER) are evaluated by theoretical analysis. Consequently, the normalized throughput of the proposed system can achieve 1.35 [bit/chip] when the number of slots per frame is 16. Furthermore, BER of the proposed system is superior to that of the conventional systems.

## 1. Introduction

Recently, there has increasing interest in optical communications such as fiber-optic communications and optical wireless communications. As a multiple access technique in the optical communication, optical code-division multiple-access (OCDMA) schemes have attracted much attention because these schemes allow multiple users to access the network asynchronously and simultaneously. In the OCDMA system using unipolar modulation, each user is assigned one particular optical spreading code. It is expected that the optical spreading code, which is assigned to each user, fulfills the following two conditions: (1) the relation between any two spreading codes is orthogonal and (2) the number of generated orthogonal codes,  $N$ , per spreading code length,  $L$ , is large, that is,  $N/L \geq 1$ . The OCDMA system with the spreading code satisfying these conditions can reduce the influence of multiple access interference (MAI) and can realize the high maximum data transmission rate (i.e., normalized throughput which is normalized by chip rate). In the conventional OCDMA systems using unipolar modulation, the optical orthogonal code (OOC), the extended prime code sequence and the pseudo orthogonal M-sequence are reported[1]-[3]. In particular, the number of generated orthogonal codes of the pseudo orthogonal M-sequence is equal to the code length. Therefore, when the OCDMA system uses the On-Off Keying (OOK) and the Multi-pulse PPM (MPPM)[4] as the unipolar modulation, the normalized throughput of the OCDMA system with the pseudo orthogonal M-sequence can achieve 1.0 [bit/chip]. However, it cannot exceed 1.0 [bit/chip] even if the number of pulses in a PPM frame increases because  $N/L = 1$ . Therefore, in order that the normalized throughput can exceed 1.0 [bit/chip], it is important to design the optical spreading code which can achieve  $N/L > 1$ .

In this paper, to realize high normalized throughput, we design the modified pseudo orthogonal M-sequence set[5]. This modified pseudo orthogonal M-sequence sets fulfills the conditions (1) and (2). Moreover, in this modified pseudo orthogonal M-sequence sets, two modified pseudo orthogonal M-

sequences are generated by one primitive M-sequence. These two modified pseudo orthogonal M-sequences also consist of zero chips and positive chips. Therefore, the modified pseudo orthogonal M-sequence sets can achieve  $N/L \approx 2$ . In this paper, we propose the OCDMA system using MPPM with the modified pseudo orthogonal M-sequence sets and show the normalized throughput of the proposed OCDMA system. Moreover, we analyze the bit error rate (BER) performance of the proposed system by taking into account the scintillation, background-noise, avalanche photo-diode (APD) noise, thermal noise and signal dependence noise.

## 2. Modified pseudo orthogonal M-sequence sets

In this section, we describe the modified pseudo orthogonal M-sequence sets. Let us consider how to design orthogonal M-sequences which are M-sequences with additional one chip. The primitive M-sequence of length  $L_M$  is defined as a sequence  $(x_1, x_2, \dots, x_{L_M})$  whose chips  $x_i (i = 1, 2, \dots, M)$  are either  $+1$  or  $-1$ . Moreover, the primitive M-sequence consists of  $(L_M - 1)/2$  negative chips and  $(L_M + 1)/2$  positive chips. Therefore, the primitive orthogonal M-sequence consists of primitive M-sequence and additional one chip, that is, the primitive orthogonal M-sequences  $OM_i (i = 1, 2, \dots, L_M)$  are

$$\begin{cases} OM_1 = \{ & x_1 & x_2 & x_3 & \cdots & x_{L_M} & -1 \} \\ OM_2 = \{ & & x_2 & x_3 & \cdots & x_{L_M} & x_1 & -1 \} \\ \vdots & & & & \vdots & & & \\ OM_{L_M} = \{ & x_{L_M} & x_1 & x_2 & \cdots & x_{L_M-1} & & -1 \} \end{cases} \quad (1)$$

where  $x_i = \pm 1 (i = 1, 2, \dots, L_M)$ . The cross-correlation value between any two orthogonal M-sequences is zero. In this orthogonal M-sequences, the sequences which replace  $-1$  by zero are denoted  $M_{A_i} (i = 1, 2, \dots, L_M)$ , and the sequences which replace  $+1$  and  $-1$  by zero and  $+1$  respectively are denoted  $M_{B_i} (i = 1, 2, \dots, L_M)$ . These  $N = 2L_M$  sequences, that are  $M_{A_i}$  and  $M_{B_i}$ , are M-sequences with on-off signaling. The sequences length of  $OM, M_A, M_B$  is  $L = L_M + 1$ . For example, when  $L_M = 7$  [chip],  $OM, M_A$  and  $M_B$  are expressed as

$$OM = \begin{bmatrix} OM_1 \\ OM_2 \\ OM_3 \\ OM_4 \\ OM_5 \\ OM_6 \\ OM_7 \end{bmatrix} = \begin{bmatrix} +1 & +1 & +1 & -1 & +1 & -1 & -1 & -1 \\ +1 & +1 & -1 & +1 & -1 & -1 & +1 & -1 \\ +1 & -1 & +1 & -1 & -1 & +1 & +1 & -1 \\ -1 & +1 & -1 & -1 & -1 & +1 & +1 & -1 \\ +1 & -1 & -1 & +1 & +1 & +1 & -1 & -1 \\ -1 & -1 & +1 & +1 & +1 & -1 & +1 & -1 \\ -1 & +1 & +1 & +1 & -1 & +1 & -1 & -1 \end{bmatrix} \quad (2)$$

$$M_A = \begin{bmatrix} M_{A1} \\ M_{A2} \\ M_{A3} \\ M_{A4} \\ M_{A5} \\ M_{A6} \\ M_{A7} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 0 & 1 & 0 & 0 & 0 \\ 1 & 1 & 0 & 1 & 0 & 0 & 1 & 0 \\ 1 & 0 & 1 & 0 & 0 & 1 & 1 & 0 \\ 0 & 1 & 0 & 0 & 1 & 1 & 1 & 0 \\ 1 & 0 & 0 & 1 & 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 & 1 & 0 & 1 & 0 \\ 0 & 1 & 1 & 1 & 0 & 1 & 0 & 0 \end{bmatrix} \quad (3)$$

$$M_B = \begin{bmatrix} M_{B1} \\ M_{B2} \\ M_{B3} \\ M_{B4} \\ M_{B5} \\ M_{B6} \\ M_{B7} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 1 & 1 & 1 \\ 0 & 0 & 1 & 0 & 1 & 1 & 0 & 1 \\ 0 & 1 & 0 & 1 & 1 & 0 & 0 & 1 \\ 1 & 0 & 1 & 1 & 0 & 0 & 0 & 1 \\ 0 & 1 & 1 & 0 & 0 & 0 & 1 & 1 \\ 1 & 1 & 0 & 0 & 0 & 1 & 0 & 1 \\ 1 & 0 & 0 & 0 & 1 & 0 & 1 & 1 \end{bmatrix} \quad (4)$$

where the  $i$ th row vector of  $OM$  is  $OM_i$ , the  $i$ th row vector of  $M_A$  is  $M_{Ai}$  and the  $i$ th row vector of  $M_B$  is  $M_{Bi}$ . These sequences have the following characteristics

$$M_A OM^T = \left(\frac{L}{2}\right) E \quad (5)$$

$$M_B OM^T = \left(-\frac{L}{2}\right) E \quad (6)$$

$$OM = M_A - M_B \quad (7)$$

where  $E$  is a unit matrix and  $x^T$  is transposed matrix of  $x$ . Therefore,  $M_{Ai}$  or  $M_{Bi}$ , that are the on-off signaling, is used as the optical spreading code at the transmitter and  $OM_i$  is used as the reference spreading code at the receiver.

### 3. The proposed OCDMA system

In the MPPM system with the modified pseudo orthogonal M-sequence sets,  $i$ th user uses the two modified pseudo orthogonal M-sequences with on-off signaling ( $M_{Ai}$  and  $M_{Bi}$ ) and the one primitive orthogonal M-sequence with polar signaling ( $OM_i$ ). Therefore, when the length of pseudo orthogonal M-sequences is  $L$  [chip], the proposed system can achieve  $L - 1$  simultaneous users. The transmitter signal is generated by the combination of multi-pulse position and two modified pseudo orthogonal M-sequences with on-off signaling ( $M_{Ai}$  and  $M_{Bi}$ ) at the transmitter. Thus, the  $\binom{M}{r} \times 2^r$  transmitter signal patterns can be formed where  $r$  is the number of pulses in a frame and  $M$  is the number of slots in a frame. This means that the number of bits per frame is  $\lfloor \log_2 \binom{M}{r} \rfloor + r$ . For example, as shown in Fig.1, a transmitter signal can be expressed when  $r = 2$  and  $M = 4$ .

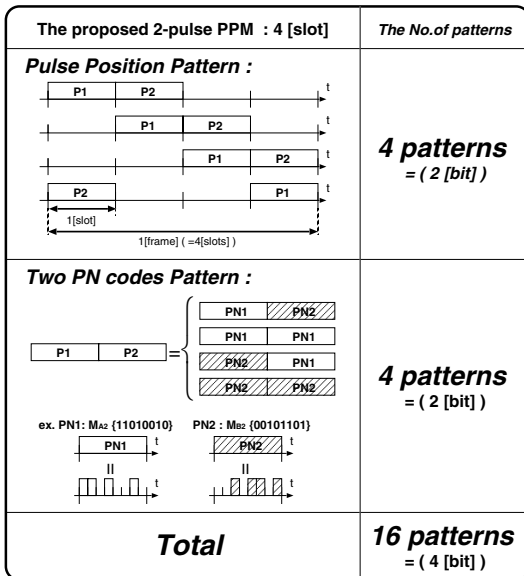


Figure 1. The transmitter signal when  $r = 2$  and  $M = 4$

Figure 2 shows the system model of the optical wireless MPPM with the modified pseudo orthogonal M-sequence sets. When source data is  $k$  [bit], correspond to  $k-2$  [bit], the multi-pulse position is chosen by pulse position modulator. Two spreading codes are selected by switching correspond to the other 2[bit].

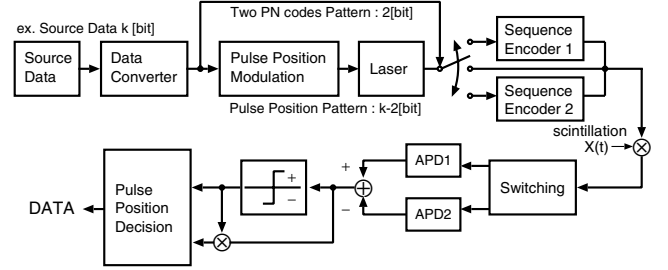


Figure 2. System model

At the receiver, high-speed switching and optical delay lines detect received optical power by the assigned primitive orthogonal M-sequence which are consisted of  $+1$  and  $-1$ . However, it is difficult to deal in a negative optical power. In this paper, two APD ( $APD_1$  and  $APD_2$ ) are used.  $APD_1$  is corresponds to  $M_{Ai}$  (i.e., a positive chips positions of  $OM_i$ ).  $APD_2$  is corresponds to  $M_{Bi}$  (i.e., a negative chips positions of  $OM_i$ ). We define that  $\mathbf{c} = (c_1, c_2, \dots, c_L)$ , where  $c_k$  is the received optical power at  $k$ th chip. The received optical power  $\mathbf{r}$  is directed to multiply  $M_{Ai}$  and  $M_{Bi}$  for correlation operation. These correlation values  $|cM_{Ai}^T|$  and  $|cM_{Bi}^T|$  are converted into the electrical signal by  $APD_1$  and  $APD_2$ , respectively. The difference between the output of  $APD_1$  and output of  $APD_2$  becomes the correlation value with reference sequence  $OM_i$  because  $OM = M_A - M_B$  in Eq.(7). In the proposed system, the symbol is declared by absolute value and polarity of the correlation value of each slot. The PPM decoder declares multi-pulse position by comparing the absolute value of the correlation value of each slot. The spreading code is declared whether the polarity of the correlation value is positive or negative. Then the final output bits corresponding to the symbol are given.

### 4. Normalized throughput

We show the normalized throughput (i.e., maximum data transmission rate). The normalized throughput is the rate of the total message bits per one frame of simultaneous users to the frame length. The proposed system can achieve  $L - 1$  simultaneous users when the length of the modified pseudo orthogonal M-sequence is  $L$  [chip]. While, the conventional system can achieve  $L_M$  simultaneous users where  $L_M$  is the length of the conventional pseudo orthogonal M-sequence[3]. Therefore, the normalized throughput of the proposed system,  $C_{pro}$ , and that of the conventional system,  $C_{con}$ , are derived respectively, as

$$C_{pro} = \frac{L-1}{L} \times \frac{\lfloor \log_2 \binom{M}{r} \rfloor + r}{M} \text{ [bit/chip]} \quad (8)$$

$$C_{con} = \frac{\lfloor \log_2 \binom{M}{r} \rfloor}{M} \text{ [bit/chip]}. \quad (9)$$

Fig.3 shows the normalized throughput versus the number of pulses in a frame when  $L = 16$  [chip] and  $M = 8, 16$  [slot]. The normalized throughput of the proposed system is better than that of the conventional MPPM system with the pseudo orthogonal M-sequences and can achieve about 1.35 [bit/chip].

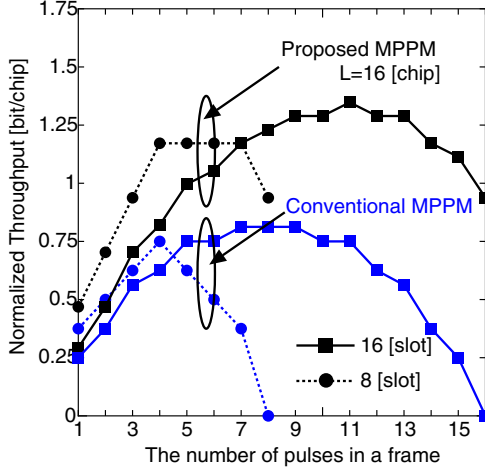


Figure 3. Normalized throughput versus the number of pulses in a frame for the proposed system ( $L = 16$ ) and the conventional MPPM system considered with  $M = 8, 16$  slots.

## 5. Theoretical analysis

In this section, we analyze the bit error (BER) rate performance of the proposed system using APD in the slot synchronous case. The output of APD is assumed to be a Gaussian distribution. The probability that a specified number of photons are absorbed from an incident optical field by an APD detector over a chip interval with  $T_c$  is given by a Poisson distribution[6].

In the optical wireless communication, we need to take into account the scintillation which influences the attenuation and the fluctuation of the received optical power. The scintillation  $X_i$  for  $i$ th user characterized by the stationary probability process. Its probability density function  $p(X_i)$  can be written as [7]

$$p(X_i) = \frac{1}{\sqrt{2\pi\sigma_s^2 X_i}} \exp \left\{ - \left( \ln X_i + \frac{\sigma_s^2}{2} \right)^2 / 2\sigma_s^2 \right\} \quad (10)$$

where the average of scintillation  $X$  is normalized to unity, and  $\sigma_s^2$  is logarithm variance. The variance  $\sigma_s^2$  is determined by the atmospheric state.

The average number of absorbed photons over  $T_c$  is

$$\lambda_s = \frac{\eta P_w}{hf} \quad (11)$$

where  $\lambda_s$  is the photon absorption rate,  $P_w$  is the received laser power,  $\eta$  is the APD efficiency,  $h$  is Planck's constant and  $f$  is the optical frequency. Through an avalanche multiplication process, the APD outputs some electrons in response to the absorption of  $\lambda T_c$  primary photons on the average. Here,  $\lambda$  represents the total photon absorption rate due to signal, background light, and APD bulk leakage current. The total photon absorption rate  $\lambda$  of the proposed system is given by

$$\lambda = \begin{cases} \frac{L}{2} \lambda_s + \frac{L}{2} \lambda_b + \frac{I_b}{e} & \text{for a mark} \\ \frac{L}{2} \frac{\lambda_s}{M_e} + \frac{L}{2} \lambda_b + \frac{I_b}{e} & \text{for a space} \end{cases} \quad (12)$$

where  $\lambda_b$  is the photon absorption rate due to actual background light ( $\lambda_b = \eta P_b / hf$  when the background noise per chip duration is  $P_b$ ),  $I_b/e$  represents the contribution of the APD bulk leakage current to the APD output and  $M_e$  is the extinction ratio of the laser diode output power in the mark and space states.

### 5.1 Bit error rate

We present the BER performance of the proposed system in the single-user case. In this paper, we define the BERs are  $P_{SER}/2$  where the  $P_{SER}$  is the symbol error rate (SER). The symbol error rate,  $P_{SER}$ , is given by

$$P_{SER} = 1 - P_{suc} \quad (13)$$

where  $P_{suc}$  is the symbol correct rate of the proposed system. We define  $M$  is the number of PPM slots in a frame,  $r$  is the number of pulses in a frame,  $q_k$  is output of the correlation value in the  $k$ th slot ( $k = 1, 2, \dots, M$ ) and  $|q_k|$  is the absolute value of the correlation value of  $k$ th slot.

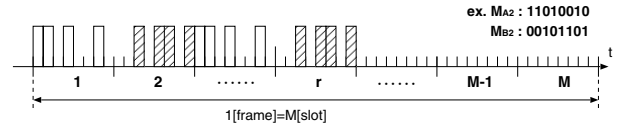


Figure 4. An example of a transmit signal pattern of the proposed system

When the desired user transmits using 1th slot, 2th slot,  $\dots$ ,  $(r-1)$ th slot and  $r$ th slot like Figure 4, the symbol correct rate of this case can be written as

$$P_{rob} [q_1 > 0, q_2 < 0, \dots, q_r < 0, (|q_1|, \dots, |q_r|) > (|q_{r+1}|, \dots, |q_M|)]$$

In this case, the desired user transmits using  $M_{A2}$  in the 1th slot. Therefore, the polarity of the  $q_1$  must be positive value. While, in the 2th slot, the polarity of the  $q_2$  must be negative value.

The symbol correct rate at the Figure 4, by the symmetry property, can be expressed as

$$\begin{aligned} P_{rob} [q_1 > 0, q_2 < 0, \dots, q_r < 0, (|q_1|, \dots, |q_r|) > (|q_{r+1}|, \dots, |q_M|)] \\ = P_{rob} [(q_1, \dots, q_r) > 0, (|q_1|, \dots, |q_r|) > (|q_{r+1}|, \dots, |q_M|)] \\ = P_{suc} \end{aligned} \quad (14)$$

Therefore, the symbol correct rate of the proposed system,  $P_{suc}$ , is given by

$$\begin{aligned} P_{suc} &= P_{rob} [(q_1, \dots, q_r) > 0, (|q_1|, \dots, |q_r|) > (|q_{r+1}|, \dots, |q_M|)] \\ &= r! \int_0^\infty p(X_0) \int_0^\infty \frac{1}{\sqrt{2\pi\sigma_1^2(X_0)}} \exp \left\{ - \frac{(q_1 - \mu_1(X_0))^2}{2\sigma_1^2(X_0)} \right\} \\ &\quad \times \int_0^{q_1} \frac{1}{\sqrt{2\pi\sigma_2^2(X_0)}} \exp \left\{ - \frac{(q_2 - \mu_2(X_0))^2}{2\sigma_2^2(X_0)} \right\} \\ &\quad \times \dots \times \int_0^{q_{r-1}} \frac{1}{\sqrt{2\pi\sigma_r^2(X_0)}} \exp \left\{ - \frac{(q_r - \mu_r(X_0))^2}{2\sigma_r^2(X_0)} \right\} \\ &\quad \times \prod_{i=r+1}^M \left[ \int_{-q_r}^{q_r} \frac{1}{\sqrt{2\pi\sigma_i^2(X_0)}} \exp \left\{ - \frac{q_i^2}{2\sigma_i^2(X_0)} \right\} dq_i \right] \\ &\quad \times dq_r \dots dq_2 dq_1 dX_0 \\ &< \int_0^\infty p(X_0) \prod_{i=r+1}^M \left[ \int_{-\infty}^\infty \frac{1}{\sqrt{2\pi\sigma_i^2(X_0)}} \exp \left\{ - \frac{q_i^2}{2\sigma_i^2(X_0)} \right\} \right. \\ &\quad \left. \times \prod_{j=1}^r \left[ \int_{|q_j|}^\infty \frac{1}{\sqrt{2\pi\sigma_j^2(X_0)}} \exp \left\{ - \frac{(q_j - \mu_j(X_0))^2}{2\sigma_j^2(X_0)} \right\} dq_j \right] dq_i \right] dX_0 \end{aligned} \quad (15)$$

where  $X_0$  is the scintillation of desired user.

In Eq(15), the average and variance of the correlation value of 1th slot,  $\mu_1(X_0)$ ,  $\sigma_1^2(X_0)$  and the variance of the correlation value of  $(r+1)$ th slot,  $\sigma_{r+1}^2(X_0)$  are derived, respectively, as

$$\mu_1(X_0) = GT_c \frac{L}{2} \left( \frac{M_e - 1}{M_e} \right) \lambda_s X_0 \quad (16)$$

$$\sigma_1^2(X_0) = G^2 F_e T_c \left[ \frac{L}{2} \left( \frac{M_e + 1}{M_e} \right) \lambda_s X_0 + L \lambda_b + \frac{2I_b}{e} \right] + \frac{2I_s T_c}{e} + \sigma_{th}^2 \quad (17)$$

$$\sigma_{r+1}^2(X_0) = G^2 F_e T_c \left[ L \frac{\lambda_s X_0}{M_e} + L \lambda_b + \frac{2I_b}{e} \right] + \frac{2I_s T_c}{e} + \sigma_{th}^2. \quad (18)$$

where  $G$  is the average APD gain,  $L$  is the length of the modified pseudo orthogonal M-sequences,  $I_s$  is the APD surface leakage current,  $F_e$  is the excess noise factor and  $\sigma_{th}^2$  is the variance of thermal noise.  $F_e$  and  $\sigma_{th}^2$  are given by

$$F_e = k_{eff} G + (1 - k_{eff}) \left( \frac{2G - 1}{G} \right) \quad (19)$$

$$\sigma_{th}^2 = \frac{4k_B T_r T_c}{e^2 R_L} \quad (20)$$

where  $k_{eff}$  is the APD effective ionization ratio,  $k_B$  is Boltzmann's constant,  $T_r$  is the receiver noise temperature and  $R_L$  is the receiver load resistor.

## 6. Numerical results

In this section, we show the result from theoretical analysis of the BER performance in the slot synchronous case. In the multi-user case, we also present the BER performance of the proposed system and that of the conventional MPPM with the pseudo orthogonal M-sequences on the worst case condition. Table 1 shows the numerical conditions for evaluation. We use typical APD parameters[7][6] and assume that the slot duration is  $1/156$  [ $\mu$ sec] and the length of modified pseudo orthogonal M-sequence,  $L$ , is 16 [chip].

Table 1. The numerical conditions

Name	Symbol	Value
Laser wavelength		830 [nm]
Background noise	$P_b$	-45 [dBm]
Quantum efficiency	$\eta$	0.6
Scintillation logarithm variance	$\sigma_s^2$	0.1
APD Gain	$G$	100
Effective ionization ratio	$k_{eff}$	0.02
Bulk leakage current	$I_b$	0.1 [nA]
Surface leakage current	$I_s$	10 [nA]
Modulation extinction ratio	$M_e$	100
Receiver noise temperature	$T_r$	1100[°K]
Receiver load resistor	$R_L$	1030[Ω]

Figure 5 shows the BER versus the received laser power per bit per frame  $P_{bit}$  for the proposed system ( $M = 4$ ,  $r = 2$ ), the binary antipodal DS/SS system, the OOK DS/SS system and the conventional MPPM system ( $M = 64$ ,  $r = 32$ ). The  $P_{bit}$  is given by

$$P_{bit} = \frac{rL}{2k} P_w \quad (21)$$

where  $k$  [bit] is the message bits per frame and  $P_w$  [dBm] is the received laser power per chip without scintillation. The four systems achieve the same normalized throughput (0.9375 [bit/slot]) and the same bit rate (156 [Mbps]). We define the BERs of the proposed system and the conventional MPPM system are  $P_{SER}/2$ . In Fig.5, the BER performance of the proposed system is the best in the four systems.

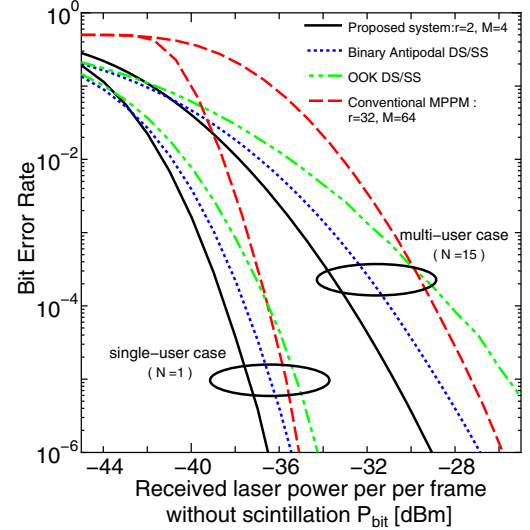


Figure 5. BER versus received laser optical power per bit per frame  $P_{bit}$  for the proposed system ( $M = 4$ ,  $r = 2$ ,  $L = 16$ ), the binary antipodal DS/SS system ( $L = 16$ ), the OOK DS/SS system ( $L = 16$ ) and the conventional MPPM system ( $M = 64$ ,  $r = 32$ ,  $L_M = 15$ ).

## 7. Conclusion

In this paper, in order to realize high normalized throughput, we have designed the modified orthogonal M-sequence sets and have proposed the OCDMA system using MPPM with the modified pseudo orthogonal M-sequence sets. Moreover, we show the result from theoretical analysis of the BER of the proposed system. Consequently, the normalized throughput of the proposed system is better than that of the conventional MPPM. Furthermore, in the same bit rate, the BER of the proposed system is better than that of the conventional systems.

## Acknowledgment

This study was supported in part by Grant-in-Aid for Scientific Research (C) in Japan.

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