

## A LONG HELICAL ANTENNA WOUND ON A DIELECTRIC ROD

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### 1. Introduction

A short helical antenna, consisting of an arm with a small number of turns (less than 2) printed on a hollow dielectric rod, has already been analyzed [1]. The analysis shows that the helix radiates a circularly polarized (CP) wave in the axial direction with a gain of approximately 7 dB.

This paper investigates the radiation characteristics of a long helical antenna (more than 2 turns). The antenna arm is printed on a hollow dielectric rod, as in [1]. The investigation is performed using the finite-difference time domain (FDTD) method based on a cylindrical coordinate system [2].

After revealing the radiation characteristics, impedance matching is considered. The impedance is matched by modifying the helical arm near the feed point. The VSWR and gain as a function of frequency for a helix with this arm modification are revealed.

### 2. Configuration and analysis method

Fig. 1 shows the configuration of a helical antenna, where the strip helical arm is printed on a hollow dielectric rod of relative permittivity  $\epsilon_r$ . The outer and inner diameters of the hollow rod are  $d_{out}$  ( $= C/\pi$ ) and  $d_{in}$ , respectively, and hence the thickness of the hollow rod is given as  $t = (d_{out} - d_{in})/2$ . The strip helical arm is specified by the following parameters: width  $w$ , initial vertical element length  $L_0$ , horizontal element length  $L_H$ , vertical element length  $L_v$ , number of turns  $n$ , and pitch  $p$ . Note that a conducting plane (ground plan (GP)) of infinite extent backs the helix.

The height of the rod above the infinite ground plane,  $h$ , equals the height of the top edge of the final arm strip segment. To simplify the discussion, the thickness  $t$  (or the inner diameter  $d_{in}$ ) and the number of turns  $n$  (and hence the height of the rod,  $h$ ) are varied, with other configuration parameters, listed in Fig. 1, remaining unchanged. Note that  $\lambda_3$  in the list is the free-space wavelength at a test frequency of 3 GHz.

Cylindrical coordinates  $(r, \theta, \phi)$  are adopted to match the configuration of the dielectric rod. Maxwell's curl equations are expressed using the cylindrical coordinates and solved using the FDTD method with Liao's absorbing boundary condition [2]. The input impedance ( $Z_{in} = R_{in} + jX_{in}$ ) is calculated using the current at the feed point,  $I_{in}$ , where the current is obtained by integrating the magnetic field  $\mathbf{H}$ , obtained by the FDTD method, around the helical arm. The radiation field  $\mathbf{E}_{rad}$  is obtained using the equivalence principle [3], in which the equivalent electric and magnetic currents on a surface enclosing the antenna are used. The gain is calculated using the obtained radiation field, together with the input power  $R_{in} |I_{in}|^2$ .

### 3. Analysis results

Fig. 2 shows the gain for a right-hand CP wave as a function of the number of turns  $n$ , where three values for the thickness of the rod,  $t$ , are used. Note that a value of  $t = 0$  corresponds to the helical arm wound in free space and a value of  $t = 0.15\lambda_3$  corresponds to the helical arm wound on a solid dielectric rod. It is found that, as the number of turns  $n$  increases, the gains of the three helices increase. It is also found that the gain is affected by the thickness  $t$ . The difference in the gains between the helices with  $t = 0$  and  $t = 0.15\lambda_3$  is approximately 0.5 dB.

As  $n$  increases, the axial ratio improves. Fig. 3 shows the axial ratio as a function of the number of turns  $n$ . The axial ratios of the three helices at  $n = 9.75$  turns are approximately 1 dB, with gains of greater than 11.5 dB.

Based on the above results, further investigation is directed towards a helix with  $n = 9.75$  turns and a rod thickness of  $t = 0.05\lambda_3$  (referred to here as the  $HX_{0.05}$ ). The input impedance of the  $HX_{0.05}$  is matched to a 50-ohm feed line by creating a matching strip section of width  $w_{mhc}$  and length  $s_{mhc}$ , as shown in Fig. 4(a). Fig. 4 (b) shows the VSWR at 3 GHz for a width of  $w_{mhc} = 2w = 0.1\lambda_3$  as a function of the length  $s_{mhc}$ . It is found that the input impedance is matched to a 50-ohm feed line at  $s_{mhc} = 0.16\lambda_3$ .

So far, a test frequency of 3 GHz has been used. Next, the frequency response of the  $HX_{0.05}$  with a matching strip section of  $(w_{mhc}, s_{mhc}) = (0.1\lambda_3, 0.16\lambda_3)$  is revealed. Fig. 5 and Fig. 6 show the VSWR and gain as a function of frequency, respectively. As seen in these figures, the VSWR and gain show wide band characteristics. The VSWR bandwidth for a VSWR= 2 criterion is 59% and the gain bandwidth for a 3-dB gain drop criterion is 48%.

### 4. Conclusions

A helical antenna, whose arm is wound on a hollow dielectric rod of relative permittivity  $\epsilon_r$ , is analyzed with the FDTD method using cylindrical coordinates. It is found that, as the thickness of the dielectric rod,  $t$ , increases, the gain decreases. It is also found that the input impedance is matched to 50 ohms by creating a matching strip section near the feed point. A helical antenna of  $(t, n, \epsilon_r) = (0.05\lambda_3, 9.75, 2.07)$ , whose arm includes the matching strip section, shows a frequency bandwidth of approximately 48% for a 3-dB gain drop criterion.

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### References

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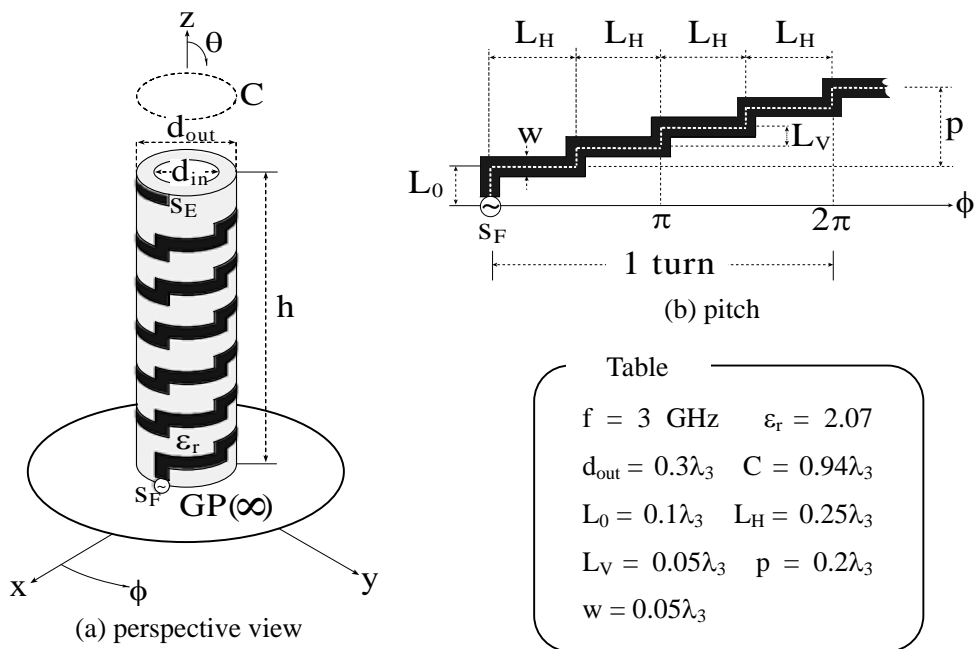


Fig. 1 A helical antenna wound on a dielectric rod.

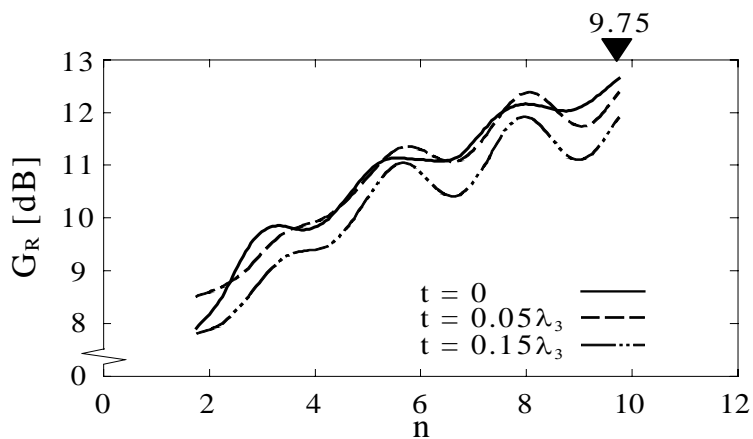


Fig. 2 Gain for a right-hand circularly polarized wave as a function of the number of turns  $n$ .

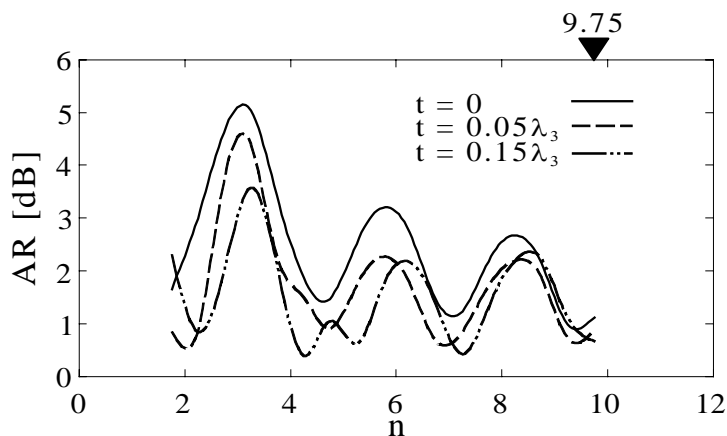


Fig. 3 Axial ratio as a function of the number of turns  $n$ .

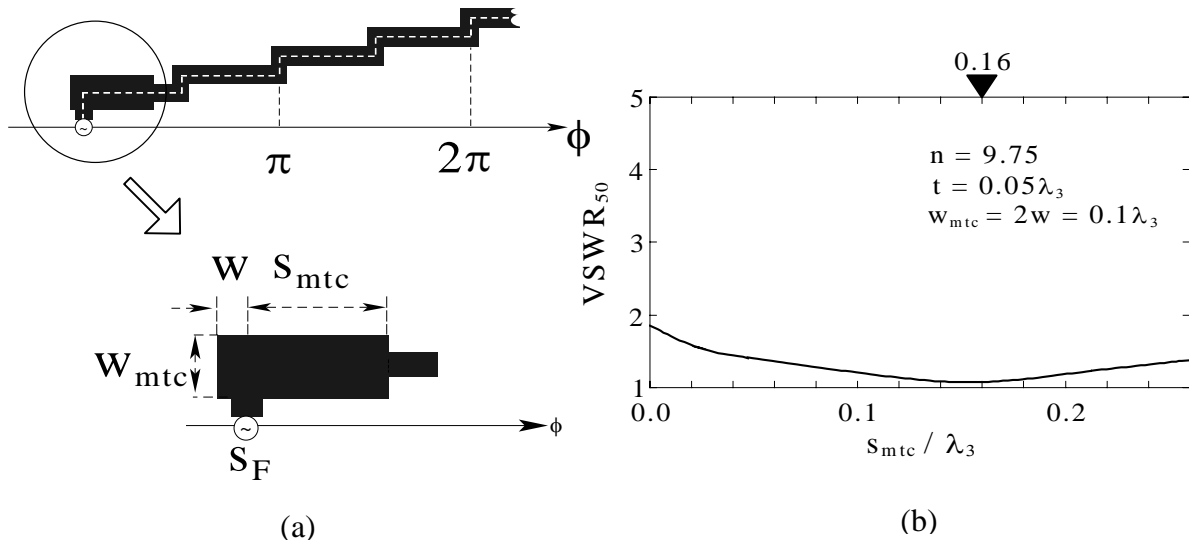


Fig. 4 VSWR as a function of length  $S_{mtc}$ .

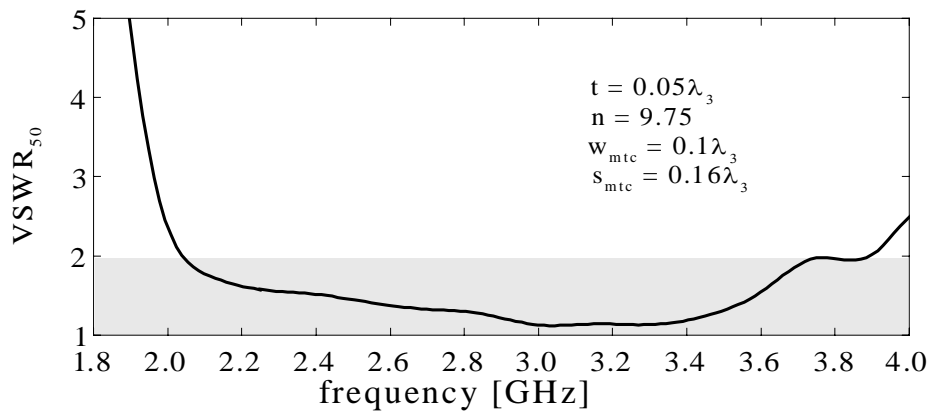


Fig. 5 Frequency response of the VSWR.

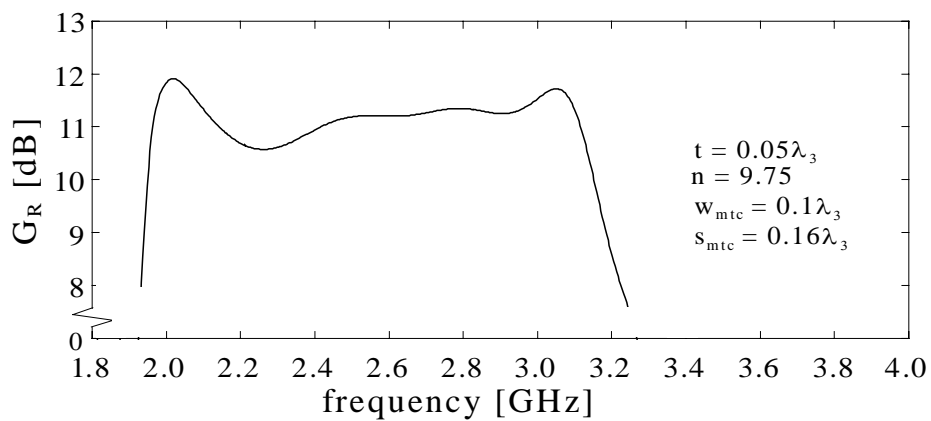


Fig. 6 Frequency response of the gain for a right-hand circularly polarized wave.