

## **An Exact solution for wave equation in lossless TEM transmission lines with time dependent media and nonlinear time dependent load(using time domain analysis)**

Ahmad cheldavi, Iran university of science and technology college of Electrical Engineering, Narmak, Tehran, Iran  
E - mail: Cheldavi @ ece.ut.ac.ir

### **Abstract**

In this paper an exact solution for wave equation in lossless TEM transmission lines with time dependent Dielectric ( $\epsilon(t)$ ) will be presented. There is no restriction about the nature of the source.

We suppose the capacitance and inductance per unit length of the line are available as respectively, time - dependent function  $C(t)$ , and constant  $L$ .

also the load may be nonlinear time - dependent load ( $Z(t)$ ).

### **1 - Introduction**

In this paper the transmission line characteristic impedance will be considered as time - dependent function  $Z(t)$ , but this time dependency is raised from  $\epsilon(t)$  or  $C(t)$  (time - dependent dielectric) and  $m$ (or  $L$ ) is constant.

To avoid from complicated computations (Transformation from frequency to time domain) we will use time domain approach directly.

Such more complicated problem was considered numerically for some simple cases such as pulse input and time - dependent load[3] but the present solution is a complete exact solution and no approximation was used.

### **2 - Differential Equations**

For a lossless transmission line as in fig.1 we have.

$$\frac{\partial v}{\partial x} = -\frac{\partial(LI)}{\partial t} \quad (1)$$

$$\frac{\partial I}{\partial x} = -\frac{\partial q}{\partial t} \quad (2)$$

$$q(x,t) = C(t) V(x,t) \quad (3)$$

Applying (3) to (1) and (2) yields

$$\frac{\partial^2 I(x,t)}{\partial x^2} = LC(t) \frac{\partial^2 I(x,t)}{\partial t^2} \quad (4)$$

$$\frac{\partial^2 q(x,t)}{\partial x^2} = LC(t) \frac{\partial^2 q(x,t)}{\partial t^2} \quad (5)$$

Eqs (4) and (5) have solutions as below

$$q(x,t) = q^+(t - \frac{x}{v}) + q^-(t + \frac{x}{v}) \quad (6)$$

$$I(x,t) = I^+(t - \frac{x}{v}) + I^-(t + \frac{x}{v}) \quad (7)$$

In which  $V(t) = \frac{1}{\sqrt{LC(t)}}$  is the wave velocity and functions with and (-) superscripts indicates forward (in +x direction) and backward (in -x direction) traveling waves. forms as (6) and (7) was solved by the author using time-domain approach [1], the only differences in this case are time dependent nature of the wave velocity and characteristic impedance of the line ( $Z(t) = \sqrt{L/C(t)}$ ). Generalization the result in [1] one can prove that the below function for voltage and current in the line satisfies (4) and (5) and also the boundary conditions in input and load terminals.

$$V(x,t) = \frac{1}{C(t)} \sum_{m=0}^{\infty} M(t - \frac{x}{v(t)} - \frac{2md}{v(t)}) [V_g C(t - \frac{x}{v(t)} - \frac{2md}{v(t)})]$$

$$\prod_{k=1}^m k_g k_l (t - \frac{x}{v(t)} - \frac{2(k-1)d}{v(t)}) + k_l (t + \frac{x}{v(t)} - \frac{d}{v(t)}) \sum_{m=1}^{\infty} M(t + \frac{x}{v(t)} - \frac{2md}{v(t)})$$

$$[V_g C(t + \frac{x}{v(t)} - \frac{2md}{v(t)})] \prod_{k=2}^m k_g k_l (t + \frac{x}{v(t)} - \frac{2(k-1)d}{v(t)}) \quad (8)$$

Because

$$I^+(t + \frac{x}{v(t)}) = \frac{1}{Z(t)C(t)} q^+(t - \frac{x}{v(t)}) \text{ and } I^-(t - \frac{x}{v(t)}) = \frac{-1}{Z_o(t)C(t)} q^-(t - \frac{x}{v(t)})$$

We can derive the below formula for current in the line.

$$I(x,t) = \frac{1}{\sqrt{LC(t)}} \left\{ \sum_{m=0}^{\infty} M(t - \frac{x}{v(t)} - \frac{2md}{v(t)}) [V_g C(t - \frac{x}{v(t)} - \frac{2md}{v(t)})] \right.$$

$$\prod_{k=1}^m k_L k_g(t - \frac{x}{v(t)} - \frac{2(k-1)d}{v(t)}) - k_L(t + \frac{x}{v(t)} - \frac{d}{v(t)}) \sum_{m=1}^{\infty} M(t + \frac{x}{v(t)} - \frac{2md}{v(t)})$$

$$[V_g C(t) + \frac{x}{v(t)} - \frac{2md}{v(t)}] \prod_{k=2}^m k_L k_g(t + \frac{x}{v(t)} - \frac{2(k-1)d}{v(t)}) \quad (9)$$

In Eqs(8) and (9)  $d$ ,  $V(t)$  and  $V_g(t)$  are respectively the line length, velocity of wave propagation and source voltage. Also  $k_g(t)$ ,  $k_L(t)$  are the reflection coefficients in input and load terminals.

$$k_g(t) = \frac{R_g - Z_0(t)}{R_g + Z_0(t)} \quad (10)$$

$$k_L(t) = \frac{Z_L(t) - Z_0(t)}{Z_L(t) + Z_0(t)} \quad (11)$$

$$M(t) = \frac{1}{2}(1 - k_g(t)) \quad (12)$$

and for simplicity we use the notation  $V_g C(x,t)$  and  $k_g k_L(x,t)$  for

$V_g(x,t)C(x,t)$  and  $k_g(x,t) k_L(x,t)$  respectively.

### 3 - Examples

In below two examples we have  $d = 400m$  and  $R_g = 50\Omega$

a)  $C(t)$  is as in Fig(2) and input is the sine pulse as in Fig(3). Voltage in the load and input terminals are plotted in (4) and (5).

b)  $C(t)$  is an Fig(2) and the load is  $R_L(t) = A \cos\omega_0 t + B$  which  $A$ ,  $B$  and  $\omega_0$  are arbitrary constant. The voltage in the load and input terminal are plotted in (6) and (7) for unit step input.

### 4 - Results and future aspects

The given formulas (8) and (9) are indeed the exact solution for the wave equation in time - dependent media and were used for TEM transmission line case. Formulas (8) and (9) are still valid even when the media is nonlinear time - dependent media. This method can be improved for other transmission lines and other wave guides which are the future work of the author.

### 5 - References

- [1] A.cheldavi, H.oraizi and M.Kamarei "Time Domain Analysis of Transmission lines" Proc. 25th EuMC, september 4.8. 1995, Bologna. Italy.
- [2] C.H.Durney, T.G stockham, Jr.K.Moten "Electromagnetic pulse propagation" Elect.Eng.Dept. univ. utah, tech. Rep, Feb.1987.

