

Position detection by Voltage Transmission between Two Printed Spiral Inductors

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Abstract— In this paper, we present a new position detection system with two printed spiral inductors(PS-Inductors). When the voltage transmission efficiency between first PS-Inductor and second PS-Inductor, which are not same PS-Inductor, is measured, value of the voltage transmission efficiency are observed with changing position. Position can be detected by using the characteristic values. We make clear to be able to construct the position detection system.

1. introduction

Recently, spiral inductor is used for chip inductor, on-chip inductor and so on. Therefore, a spiral antenna is used for RFID etc.. The spiral inductors and spiral antennas are developed rapidly. Especially, spiral antennas are used to RFID etc[1]-[3]. However, mutual inductance between two or more spiral inductors is not often used.

In this study, voltage transmission efficiencies between two printed spiral inductors (PS-Inductors) are investigated. If an alternate current of an arbitrary frequency is given to the primary PS-Inductor, an alternate current which has the same cycle of primary PS-Inductor is generated at the secondary PS-Inductor by the electromagnetic induction[4],[5]. Transmission efficiency is obtained from voltages of primary PS-Inductor and secondary PS-Inductor.

Firstly, voltage transmission efficiency between two same PS-Inductors is investigated as changing frequency. Next, by shape, size and the location of the secondary PS-Inductor is changed, transmission efficiencies are investigated. Finally, the new position detection system is constructed based on the above-mentioned measurement result. When secondary inductor at an arbitrary coordinate is existed, the voltage transmission efficiency($v1_{ik}$) is measured. The secondary inductor is rotated by an arbitrary angle. and the voltage transmission efficiency($v2_{ij}$) is measured. If a combination of $v1_{ik}$ and $v2_{ik}$ differs from combinations of $v1_{lm}$ and $v2_{lm}$ of all coordinates, position of secondary inductor can be determined by using $v1$ and $v2$, It is made clear that an angle, which the combination of $v1_{ik}$ and $v2_{ik}$ is unique value, exists. We make clear to be able to construct the position detection system.

2. Measurement of Inductance

The inductance of the PS-Inductor is given from following circuit (see Fig.1). This circuit shows the Colpitts oscillator. In setting up the circuit equation in this circuit, and assuming imaginary part =0, the following equations (1) are given.

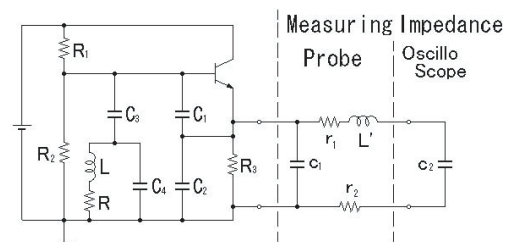


Figure 1: Circuit of inductance measurement

$$L = \frac{1 + \sqrt{1 - 4\eta^2 R^2}}{2\omega\eta} \quad (1)$$

where

$$\eta = (\omega C_4 + \frac{-\zeta}{\epsilon + \zeta})$$

$$\alpha = 1 - \omega^2(r_1 + r_2)R_3c_2(c_1 + C_2) - \omega^2c_2L$$

$$\beta = R_3(c_1 + c_2 + C_2) + c_2(r_1 + r_2) - \omega^2LR_3c_2(c_1 + C_2)$$

$$\gamma = R_3 - \omega^2c_2R_3L$$

$$\delta = (r_1 + r_2)c_2R_3$$

$$\epsilon = \frac{\alpha R_3 + \omega^2\beta\gamma}{\alpha^2 + \omega^2\beta^2}$$

$$\zeta = -\frac{1}{\omega}(\frac{1}{C_1} + \frac{1}{C_3}) + \frac{\omega(\alpha\gamma - \beta R_3)}{\alpha^2 + \omega^2\beta^2}$$

3. Experiment

3.1. Transmission Efficiency of Same Inductors

Two PS-Inductors which have same characteristics are overlapped at a distance of 1.6[mm]. Voltage transmission efficiency between the primary and the secondary PS-Inductors is observed by using a circuit of Fig.2. The parameter is each $L1 = L2 = 11.0[\mu H]$, and $C2 = 109[nF]$. The voltage transmission efficiency is obtained as follows.

$$\text{Voltage Transmission Efficiency} = \frac{V_2}{V_1} . \quad (2)$$

An observed phenomenon is shown in Fig.3. Vertical axis means voltage transmission efficiency, and horizontal axis means frequency. Maximum voltage transmission efficiency is observed when frequency is around 11.8[MHz]. Although two PS-Inductors are same parameters, maximum output voltage can be generated seven times of input voltage.

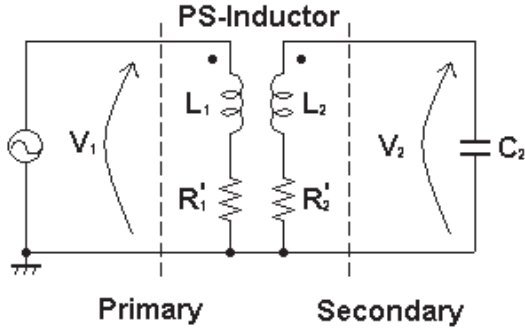


Figure 2: Circuit of measurement (same inductors).

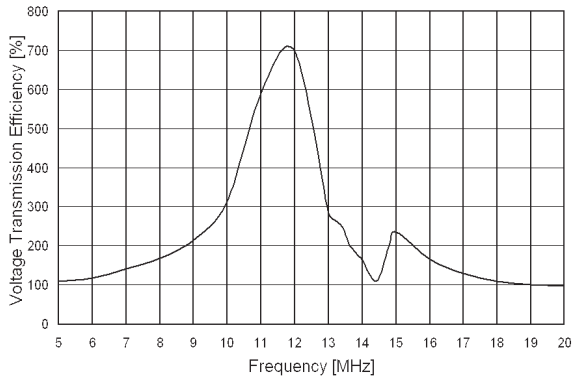


Figure 3: Voltage transmission efficiency between two same PS-Inductors.

3.2. Resonance Frequency

We prepare the PS-Inductors of the following specifications.

1. Primary inductor (see Fig.4)

Maximum diameter(D_{max}) = 92.0[mm]
 Minimum diameter(D_{min}) = 4.0[mm]
 Number of half turns = 89[turns]
 Width of conductor = 0.2[mm]
 Distance between conductors = 0.8[mm]

2. Secondary inductor (see Fig.5)

As the secondary inductors, some half-circles which diameters respectively differ are prepared. The diameters (D) of half-circles are shown in Table 1.

C_2 is coupled to the secondary inductor (see Fig.2). The capacity of C_2 is set 106[nF] which is much larger than capacitance of a probe because of disregarding the influence

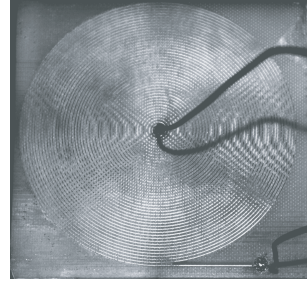


Figure 4: Primary inductor.

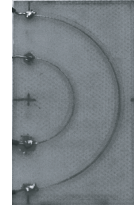


Figure 5: Sample of secondary inductor.

Table 1: Diameters of half circle.

Diameter (D) [mm]	Proportion to D_{max} [%]
23.0	25
46.0	50
69.0	75
92.0	100

of the capacitance of the probe. Centers of the primary inductor and secondary inductor are set to same location and proportion of secondary voltage to primary voltage is investigated changing frequency of input signal. Fig.6 shows the results. Theoretical resonance frequency is given by this equation.

$$f = \frac{1}{2\pi\sqrt{LC}} . \quad (3)$$

Table2 shows the theoretical value and the experimental result of resonance frequency.

We can observe that experimental results resemble to values of theory. The following measurements are used resonance frequencies of experimental result of Table 2.

3.3. Transmission Efficiency

3.3.1. Method of measurement

The transmission efficiency between primary and secondary is measured changing position of secondary half

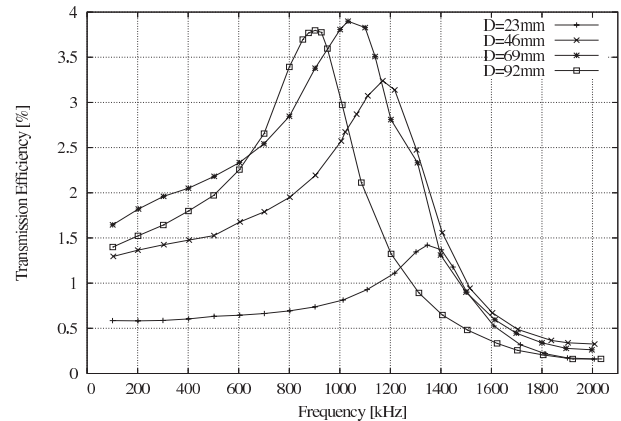


Figure 6: Frequency characteristic

Table 2: Resonance frequency of each inductor

Diameter	Measurements	Theoretically value
23.0	1.4	1.4
46.0	1.2	1.1
69.0	1.1	0.99
92.0	0.90	0.88
[mm]	[MHz]	[MHz]

circle inductor. The methods of changing the position is as follows:

1. The center of primary inductor and the center of secondary inductor are matched, and the center of primary is set as original point, and, x-axis and y-axis are provided.
2. The secondary inductor is moved at intervals of 5.0[mm] along x-axis and y-axis respectively.

3.3.2. Measurement result

The measurement results of Sec.3.3.1 are shown in Figs.8-11. The (a) of each Figs.8-11 expresses result of mapping to xz-plane.

When $y=0$, voltage proportions of each secondary inductor to primary inductor are shown in Fig.7. We can observe that voltage proportion depends on diameter of the secondary inductor.

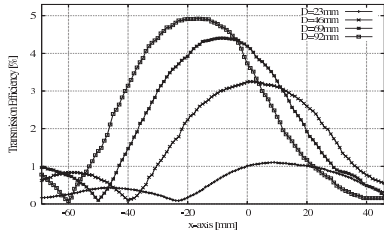
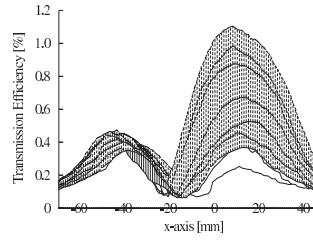


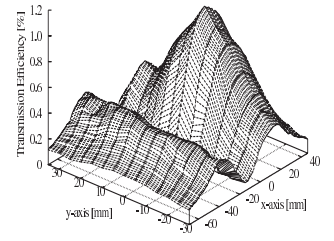
Figure 7: Voltage proportion of secondary to primary ($y=0$).

Six phenomena are observed as follows:

1. Maximum proportion of voltage exists on y-axis without influence of diameter of secondary PS-Inductor.
2. The second heights of local maximum are almost same.
3. A coordinate of maximum voltage proportion is changed to depend on diameter of secondary PS-Inductor.
4. A line where the voltage proportion is around zero existed.
5. Value of voltage proportion depend on the diameter of secondary PS-Inductor very much.
6. When $D=23$ [mm] and $y=-25$ [mm], line of minimum value is observed. We can not observe minimum value as other diameter of secondary PS-Inductors.

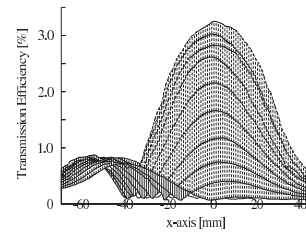


(a) Voltage proportion of secondary to primary (mapping to xz-plane).

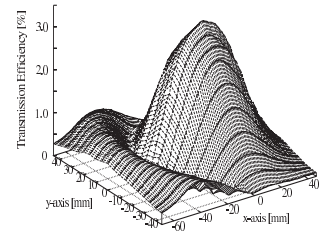


(b) Voltage proportion of secondary to primary.

Figure 8: $D=23.0(25\%)$ [mm].

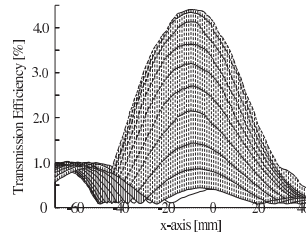


(a) Voltage proportion of secondary to primary (mapping to xz-plane).

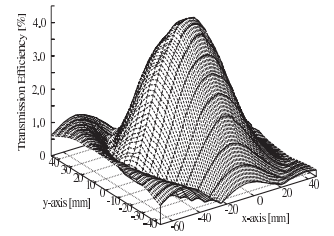


(b) Voltage proportion of secondary to primary.

Figure 9: $D=46.0(50\%)$ [mm].

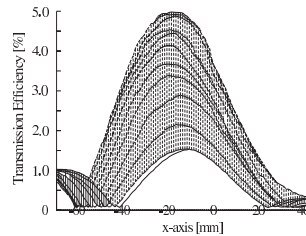


(a) Voltage proportion of secondary to primary (mapping to xz-plane).

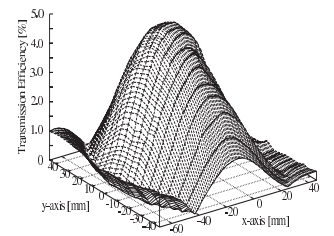


(b) Voltage proportion of secondary to primary.

Figure 10: $D=69.0(75\%)$ [mm].



(a) Voltage proportion of secondary to primary (mapping to xz-plane).



(b) Voltage proportion of secondary to primary.

Figure 11: $D=92.0(100\%)$ [mm].

3.4. Position detection

A system of position detection is constructed by using the results of the Sec.3.3.2. A voltage transmission efficiency of arbitrary coordinates (x, y) is expressed $v_1(x, y)$. A voltage transmission efficiency at (x, y) is expressed $v_2(x, y)$ when the secondary inductor is rotated an arbitrary angle. If a combination of $v_1(i, k)$ and $v_2(i, k)$ is unique for combinations at all other positions, the system of position detection can be constructed. We consider v_1v_2 -plane which is mapped from xy -plane. When $(v_1(0, 0), v_2(0, 0))$ is the reference point, the vectors are expressed as follows:

$$(v_{1ik}, v_{2ik}) = (v_1(i, k) - v_1(0, 0), v_2(i, k) - v_2(0, 0)) \quad (4)$$

where

$$-\frac{D_{max}}{2} \leq i \leq \frac{D_{max}}{2}, \quad -\frac{D_{max}}{2} \leq k \leq \frac{D_{max}}{2}. \quad (5)$$

When Eq.6 is satisfied, a combination of v_{1ik} and v_{2ik} is unique.

$$v_{1ik} \neq v_{1lm} \quad \text{or} \quad v_{2ik} \neq v_{2lm} \quad (i \neq l \text{ or } k \neq m). \quad (6)$$

We investigate the arbitrary angle which satisfies these requirements. These requirements are satisfied when the secondary inductor is rotated 180 degrees and the diameter of secondary inductor equals 46[mm](see Fig. 12).

4. Conclusion

In this study, voltage transmission between two PS-Inductors were investigated and we made clear to be able to construct the position detection system.

When two same PS-Inductors were matched and frequency was changed, very interesting phenomenon of voltage transmission efficiency was observed. When frequency was around 11.7[MHz], maximum voltage transmission efficiency was able to be generated. The maximum output voltage of the input voltage was generated seven times.

Further, voltage transmission efficiency between primary and secondary PS-Inductors was investigated when each diameter was $D = 23[mm]$, $46[mm]$, $69[mm]$ and $92[mm]$. Six phenomena were observed.

When the secondary inductor is rotated 180 degrees and the diameter of secondary inductor equals 46[mm], a position of secondary PS-Inductor was able to be detected by measuring $v_1(i, k)$ and $v_2(i, k)$.

Acknowledgments

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References

[1] Schmuckle, F.J., "The method of lines for the analysis of rectangular spiral inductors [in MMICs]," Microwave Theory and Techniques, IEEE Transactions on, Vol.41, Issue6, pp.1183-1186, June-July 1993.

x [mm]	y [mm]	v1 [V]	v2 [V]	x [mm]	y [mm]	v1 [V]	v2 [V]	x [mm]	y [mm]	v1 [V]	v2 [V]	x [mm]	y [mm]	v1 [V]	v2 [V]
-45	-45	0.6925	0.103	5	-20	2.11	0.628	0	0	2.735	0.1655	-5	40	0.1315	0.403
-40	-45	0.736	0.099	10	-20	1.97	0.628	0	0	2.705	0.478	0	40	0.203	0.3525
-35	-45	0.6905	0.1115	15	-20	1.705	0.5	10	10	2.58	0.375	5	40	0.2375	0.2875
-30	-45	0.625	0.1155	20	-20	1.455	0.69	15	10	2.36	0.515	10	40	0.2415	0.225
-25	-45	0.519	0.103	25	-20	1.135	0.83	20	10	2.03	0.655	15	40	0.222	0.272
-20	-45	0.4185	0.1065	30	-20	0.83	1.13	25	10	1.595	0.99	20	40	0.175	0.219
-15	-45	0.309	0.097	35	-20	0.61	1.49	30	10	1.17	1.355	25	40	0.1405	0.178
-10	-45	0.2	0.0875	40	-20	0.455	2.045	35	10	0.845	1.725	30	40	0.1	0.122
-5	-45	0.1065	0.103	45	-20	0.33	2.345	40	10	0.595	2.08	35	40	0.0845	0.64
0	-45	0.0655	0.1565	45	-15	0.215	2.47	45	10	0.42	2.315	40	40	0.0815	0.7125
5	-45	0.094	0.228	40	-15	0.295	2.5	45	15	0.64	2.515	45	40	0.0905	0.7375
10	-45	0.122	0.3125	35	-15	0.28	2.39	40	15	0.75	2.615	45	45	0.0765	0.8875
15	-45	0.1175	0.403	30	-15	0.655	2.22	35	15	0.22	2.865	40	45	0.2405	0.8815
20	-45	0.103	0.5125	25	-15	1.08	1.905	30	15	0.61	2.375	35	45	0.2375	0.8845
25	-45	0.094	0.6125	20	-15	1.595	1.485	25	15	1.03	1.985	30	45	0.7	0.2845
30	-45	0.0845	0.7	15	-15	1.985	1.03	20	15	1.485	1.595	25	45	0.6125	0.194
35	-45	0.0845	0.7375	10	-15	2.375	0.61	15	15	1.905	1.08	20	45	0.5125	0.094
40	-45	0.0815	0.7405	5	-15	2.565	0.22	10	15	2.22	0.655	15	45	0.403	0.1175
45	-45	0.0875	0.7065	0	-15	2.615	0.375	5	15	2.39	0.28	10	45	0.3125	0.122
45	-40	0.7375	0.0905	5	-15	2.515	0.64	0	15	2.5	0.295	5	45	0.228	0.094
40	-40	0.7125	0.0815	10	-15	2.315	0.42	5	15	2.47	0.515	5	45	0.1565	0.0655
35	-40	0.64	0.0845	15	-15	2.08	0.595	10	15	2.345	0.33	5	45	0.103	0.1065
30	-40	0.522	0.1	20	-15	1.725	0.845	15	15	2.045	0.455	10	45	0.0875	0.2
25	-40	0.378	0.1405	25	-15	1.335	1.17	20	15	1.69	0.61	15	45	0.097	0.303
20	-40	0.219	0.175	30	-15	0.99	1.595	25	15	1.33	0.83	20	45	0.1065	0.4185
15	-40	0.072	0.222	35	-15	0.695	2.03	30	15	0.97	1.425	25	45	0.103	0.519
10	-40	0.225	0.2415	40	-15	0.515	2.36	35	15	0.69	1.455	30	45	0.1155	0.625
5	-40	0.2875	0.2375	45	-15	0.375	2.58	40	15	0.5	1.705	35	45	0.1115	0.6905
0	-40	0.4625	0.203	45	-10	0.478	2.705	45	15	0.36	1.97	40	45	0.1095	0.728
5	-40	0.403	0.1315	40	-10	0.1655	2.735	45	20	0.628	2.11	45	45	0.103	0.6925
10	-40	0.397	0.135	35	-10	0.26	2.47	40	20	0.472	2.16	45	45	0.103	0.6925
15	-40	0.3625	0.25	30	-10	0.79	2.47	35	20	0.169	2.065	45	45	0.103	0.6925
20	-40	0.3065	0.385	25	-10	1.285	2.205	30	20	0.315	1.875	45	45	0.103	0.6925
25	-40	0.245	0.45	20	-10	1.89	2.02	25	20	0.47	1.665	45	45	0.103	0.6925
30	-40	0.203	0.555	15	-10	2.315	1.555	20	20	0.685	1.39	45	45	0.103	0.6925
35	-40	0.169	0.615	10	-10	2.61	1.09	15	20	1.055	0.965	45	45	0.103	0.6925
40	-40	0.1375	0.815	5	-10	2.75	0.26	10	20	1.71	0.42	45	45	0.103	0.6925
45	-40	0.1125	0.815	0	-10	2.825	0.26	5	20	1.915	0.15	45	45	0.103	0.6925
45	-35	0.7405	0.1	5	-10	2.805	0.5	0	20	1.98	0.3815	45	45	0.103	0.6925
40	-35	0.6905	0.14	10	-10	2.705	0.455	5	20	2.085	0.603	45	45	0.103	0.6925
35	-35	0.597	0.17	15	-10	2.47	0.625	10	20	1.97	0.25	45	45	0.103	0.6925
30	-35	0.445	0.215	20	-10	2.1	0.89	15	20	1.705	0.24	45	45	0.103	0.6925
25	-35	0.2565	0.315	25	-10	1.67	1.345	20	20	1.405	0.475	45	45	0.103	0.6925
20	-35	0.1345	0.405	30	-10	1.245	1.865	25	20	1.065	0.765	45	45	0.103	0.6925
15	-35	0.3405	0.515	35	-10	0.875	2.235	30	20	0.795	0.86	45	45	0.103	0.6925
10	-35	0.5125	0.595	40	-10	0.625	2.595	35	20	0.545	1.1	45	45	0.103	0.6925
5	-35	0.647	0.61	45	-10	0.405	2.8	40	20	0.42	1.32	45	45	0.103	0.6925
0	-35	0.722	0.585	45	-5	0.405	2.955	45	20	0.295	1.515	45	45	0.103	0.6925
5	-30	0.7405	0.1	5	-5	0.515	2.905	45	25	0.75	1.45	45	45	0.103	0.6925
10	-30	0.708	0.36	35	-5	0.51	2.905	40	25	0.6	1.655	45	45	0.103	0.6925
15	-30	0.6405	0.21	30	-5	0.985	2.75	35	25	0.365	1.565	45	45	0.103	0.6925
20	-30	0.514	0.315	25	-5	1.41	2.4	30	25	0.1	1.385	45	45	0.103	0.6925
25	-30	0.425	0.315	20	-5	2.095	1.955	25	25	0.33	1.135	45	45	0.103	0.6925
30	-30	0.3315	0.5	15	-5	2.515	1.42	20	25	0.68	0.805	45	45	0.103	0.6925
35	-30	0.265	0.67	10	-5	2.78	0.875	15	25	0.885	0.47	45	45	0.103	0.6925
40	-30	0.1875	0.765	5	-5	2.945	0.397	10	25	1.235	0.15	45	45	0.103	0.6925
45	-30	0.147	0.82	0	-5	2.93	0.5	5	25	1.42	0.28	45	45	0.103	0.6925
45	-30	0.71	0.17	5	-5	2.955	0.51	0	25	1.54	0.49	45	45	0.103	0.6925
40	-30	0.6	0.225	10	-5	2.795	0.575	5	25	1.52	0.68	45	45	0.103	0.6925
35	-30	0.43	0.32	15	-5	2.565	0.845	10	25	1.445	0.205	45	45	0.103	0.6925
30	-30	0.225	0.44	20	-5	2.25	1.095	15	25	1.25	0.28	45	45	0.103	0.6925
25	-30	0.169	0.58	25	-5	1.78	1.525	20	25	1.04	0.35	45	45	0.103	0.6925
20	-30	0.445	0.705	30	-5	1.28	2.14	25	25	0.835	0.49	45	45	0.103	0.6925
15	-30	0.68	0.82	35	-5	0.875	2.595	30	25	0.635	0.65	45	45	0.103	0.6925
10	-30	0.9	0.9	40	-5	0.595	2.89	35	25	0.465	0.805	45	45	0.103	0.6925
5	-30	1.065	1.08	45	-5	0.405	3.11	40	25	0.335	0.96	45	45	0.103	0.6925
0	-30	1.15	1.085	45	0	0.445	3.205	45	25	0.28	1.1	45	45	0.103	0.6925
1	-30	1.155	0.985	40	0	0.51	3.24	45	30	0.405	1.115	45	45	0.103	0.6925
2	-30	1.165	0.815	35	0	0.43	3.11	40	30	0.705	1.135	45	45	0.103	0.6925
3	-30	1.165	0.58	30	0	0.555	2.945	35	30	0.525	1.135	45	45	0.103	0.6925
4	-30	1.17	0.335	25	0	1.635	2.655	30	30	0.315	1.165	45	45	0.103	0.6925
5	-30	1.18	0.315	20	0	2.235	2.235	25	30	0.115	1.18	45	45	0.103	0.6925
6	-30	1.165	0.265	15	0	2.655	1.8	20	30	0.335	1.17	45	45	0.103	0.6925
7	-30	1.155	0.525	10	0	2.945	1.055	15	30	0.58	1.165	45	45	0.103	0.6925
8	-30	1.135	0.705	5	0	3.11	0.43	10	30	0.815	1.165	45	45	0.103	0.6925
9	-30	1.11	0.805	0	0	3.085	0	5	30	0.985	1.165	45	45	0.103	0.6925
10	-30	1.1	0.25	5	0	3.205	0.445	0	30	1.085	1.135	45	45	0.103	0.6925
15	-30	1.065	0.33	10	0	3.13	0.505	5	30						