

Distribution of Energy Flow by Dielectric Waveguide with Rhombic Dielectric Structure along a Middle Layer

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1. Introduction

Light propagation in periodic structure waveguide such as photonic crystals^[1] waveguide is both theoretical and practical interest in many areas of physics and engineering. As these applications, there are devices such as an optical resonator, an optical waveguide filter, and integrated optical devices^[2]. Consequently, in the design of photonic crystal structures with periodic constants identical to the optical wavelength, it is important to investigate the stop band region or photonic band-gaps. Though it is not analyzed the propagation constants in detailed in Bragg region, many analysis results are shown only the distribution of the electromagnetic fields by using the FDTD method^[2] or another numerical techniques^{[3]-[6]}.

In recent paper^[7], we analyzed the propagation characteristics of dielectric waveguide composed of dielectric circular cylinders array loaded with dielectric circular cylinders or dielectric triangular cylinders along a middle layer. In addition, we also investigated the distribution of energy flow at the guided area for the case of dielectric circular cylinders and dielectric triangular cylinders along a middle layer for TE_0 and TM_0 modes. As these results, we denoted that it can be concentrated the energy by loaded with dielectric circular cylinders along a middle layer for TE_0 mode, and loaded with dielectric triangular cylinders along a middle layer for TM_0 mode.

However, the distribution of energy flow in the case of asymmetric structure such as triangular cylinders cannot be obtained sufficient results for TM_0 mode. On the other hand, the confinement effects in the defect area cannot be obtained compared with dielectric circular cylinders for TE_0 mode. Consequently, we considered that the energy is carried outside by the influence of asymmetric structure.

In this paper, we have analyzed the distribution of energy flow for dielectric waveguide introduced as defect layers composed of dielectric circular cylinders loaded with symmetric structure such as rhombic dielectric structure along a middle layer for both TM_0 and TE_0 modes by using the propagation constants of the guided area and investigated the effect of rhombic dielectric structure compared with dielectric circular cylinders or dielectric triangular cylinders for TE_0 and TM_0 mode, respectively. As numerical results, it is shown that we can be obtained the effectiveness of proposed analytical model for TM_0 mode^[8].

2. Method of Analysis

We consider the dielectric waveguide with rhombic dielectric structure along a middle layer as shown in Fig.1 (a). The structure ($D = Ld$) shown in the figure is periodic with a period p along the z direction and uniform in the y -direction. The configuration shown ($L = 5$) has dielectric circular cylinders with radius a and $d_1/2$ in the x - and z -directions, respectively. The thickness of each layer is defined by d . The permittivity of regions S_1 and S_3 are denoted by ϵ_0 and that of circular cylinder array in the periodic length is denoted by ϵ_a , ϵ_b , and ϵ_3 . The middle layer region has only rhombic dielectric structure with parameters b and c in the x - and z -directions and dielectric constants $\epsilon_3^{(m)}$. The permeability is assumed to be μ_0 in all regions. The time dependence $\exp(-i\omega t)$ in the field expression will be omitted. In the formulation, the TM mode (the magnetic field has only the y -component) is discussed, and TE mode (the electric field has only the y -component) only numerical results are presented. The magnetic fields in the regions S_1 ($x \geq 0$) and S_3 ($x \leq -D$) are expressed as^[7,8]

$$H_y^{(1)} = e^{i\gamma z} \sum_{n=-N}^N r_n \exp\{ik^{(n)}x + i2n\pi z/p\}, \quad (1)$$

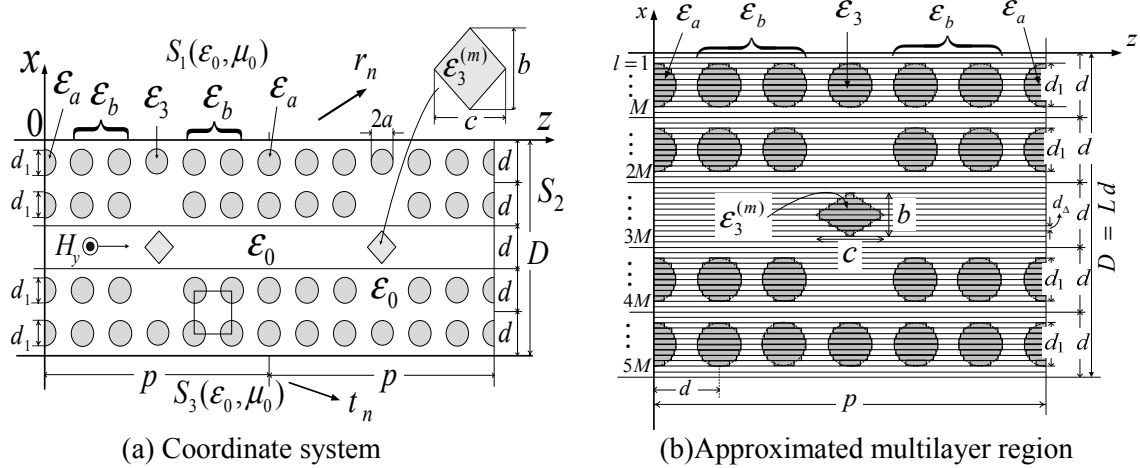


Fig.1 Structure of dielectric waveguide with rhombic dielectric structure along a middle layer

$$H_y^{(3)} = e^{i\gamma z} \sum_{n=-N}^N t_n \exp\{-ik^{(n)}(x+D) + i2n\pi z/p\}, \quad (2)$$

$$k^{(n)} \triangleq \sqrt{k_0^2 - (\gamma + 2n\pi/p)^2}, \quad k_0 \triangleq \omega\sqrt{\epsilon_0\mu_0} = 2\pi/\lambda, \quad (3)$$

where $\gamma (\triangleq \beta + i\alpha, \alpha > 0)$ and $k^{(n)}$ are the propagation constants in the z - and x -directions, respectively. k_0 is the wave number and λ is the wavelength in free space. r_n and t_n are unknown coefficients to be determined from boundary conditions. The sign of $k^{(n)}$ are given by the radiation condition in guiding problem^[7]. In the region S_2 ($-D < x < 0$), the first layer ($-d < x < 0$) is divided into M thin layers and the profile in each layer ($d_\Delta \triangleq d/M$) is approximated by step index profile $\epsilon^{(l)}(z)$ as shown in Fig.1 (b). Using the eigenvalue $h_v^{(l)}$ and eigenvector $u_{v,n}^{(l)}$ founded from eigenvalue equation^[7,8], the electromagnetic fields can be expanded as finite Fourier series.

$$H_y^{(2,l)} = e^{i\gamma z} \sum_{\nu=1}^{2N+1} [A_\nu^{(l)} e^{-ih_\nu^{(l)}\{x+(l-1)d_\Delta\}} + B_\nu^{(l)} e^{ih_\nu^{(l)}(x+ld_\Delta)}] \sum_{n=-N}^N u_{\nu,n}^{(l)} e^{i\frac{2n\pi z}{p}}, \quad 1 \leq l \leq M, \quad (4)$$

$$E_x^{(2,l)} \triangleq \{i\omega\epsilon^{(l)}(z)\}^{-1} (\partial H_y^{(2,l)} / \partial z), \quad E_z^{(2,l)} \triangleq \{-i\omega\epsilon^{(l)}(z)\}^{-1} (\partial H_y^{(2,l)} / \partial x), \quad (5)$$

where $A_\nu^{(l)}, B_\nu^{(l)}$ are unknown coefficients to be determined from boundary conditions. Using the boundary conditions at $x = -ld_\Delta$ ($l = 1 \sim M-1$), we can be obtained the matrix relation between $\mathbf{A}^{(1)}, \mathbf{B}^{(1)}$ and $\mathbf{A}^{(M)}, \mathbf{B}^{(M)}$ ^[7,8].

$$\begin{pmatrix} \mathbf{A}^{(1)} \\ \mathbf{B}^{(1)} \end{pmatrix} = \begin{pmatrix} \mathbf{S}_1^{(1)} & \mathbf{S}_2^{(1)} \\ \mathbf{S}_3^{(1)} & \mathbf{S}_4^{(1)} \end{pmatrix} \begin{pmatrix} \mathbf{S}_1^{(2)} & \mathbf{S}_2^{(2)} \\ \mathbf{S}_3^{(2)} & \mathbf{S}_4^{(2)} \end{pmatrix} \cdots \begin{pmatrix} \mathbf{S}_1^{(M)} & \mathbf{S}_2^{(M)} \\ \mathbf{S}_3^{(M)} & \mathbf{S}_4^{(M)} \end{pmatrix} \begin{pmatrix} \mathbf{A}^{(M)} \\ \mathbf{B}^{(M)} \end{pmatrix} = \begin{pmatrix} \mathbf{S}_1 & \mathbf{S}_2 \\ \mathbf{S}_3 & \mathbf{S}_4 \end{pmatrix} \begin{pmatrix} \mathbf{A}^{(M)} \\ \mathbf{B}^{(M)} \end{pmatrix}, \quad (6)$$

For the first layers to the middle layer, we can get the matrix relation between $\mathbf{A}^{(1)}, \mathbf{B}^{(1)}$ and $\mathbf{A}^{(3M)}, \mathbf{B}^{(3M)}$, between $\mathbf{A}^{(3M)}, \mathbf{B}^{(3M)}$ and $\mathbf{A}^{(5M)}, \mathbf{B}^{(5M)}$ as following equation ^[7,8], respectively:

$$\begin{pmatrix} \mathbf{A}^{(1)} \\ \mathbf{B}^{(1)} \end{pmatrix} = \begin{pmatrix} \mathbf{S}_1^{(U)} & \mathbf{S}_2^{(U)} \\ \mathbf{S}_3^{(U)} & \mathbf{S}_4^{(U)} \end{pmatrix} \begin{pmatrix} \mathbf{A}^{(3M)} \\ \mathbf{B}^{(3M)} \end{pmatrix}, \quad \begin{pmatrix} \mathbf{A}^{(3M)} \\ \mathbf{B}^{(3M)} \end{pmatrix} = \begin{pmatrix} \mathbf{S}_1^{(L)} & \mathbf{S}_2^{(L)} \\ \mathbf{S}_3^{(L)} & \mathbf{S}_4^{(L)} \end{pmatrix} \begin{pmatrix} \mathbf{A}^{(5M)} \\ \mathbf{B}^{(5M)} \end{pmatrix}. \quad (7)$$

Rearranging the unknown coefficients with respect to $\mathbf{A}^{(3M)}$ in the middle layer, substituting Eq.(7) into the boundary conditions at $x = 0$ and $x = -D$, we can be obtained the following equation^[7,8]:

$$\mathbf{W} \cdot \mathbf{A}^{(3M)} = \mathbf{0}, \quad (8)$$

For a nontrivial solution to exist in Eq.(8), we have the following characteristics equation^[7,8]:

$$\det(\mathbf{W}) = 0. \quad (9)$$

The propagation constants γ can be evaluated by utilizing the Muller's method^[7,8] to calculate in Eq.(9). To analyze the distribution of energy flow by using the propagation constant γ founded from in Eq.(9), the Poynting vector is defined by following equation:

$$\mathbf{S} \triangleq \mathbf{a}_x S_x + \mathbf{a}_z S_z, \quad (10)$$

where \mathbf{a}_x and \mathbf{a}_z are the unit vector in the x and z -directions, respectively.

In the electromagnetic fields of the middle layer, the unknown coefficients are given by the ratio of

$A_{v \neq 1}^{(l)} / A_{v=1}^{(l)}$ from Eq.(8). Therefore, we normalized coefficients $A_{v=1}^{(l=(M+1)/2)} = 1$ as following equation:

$$H_y^{(2,l)} = e^{i\gamma z} \sum_{v=1}^{2N+1} [A_v^{(l)} e^{-ih_v^{(l)} \{x+(l-1)d_\Delta\}} + B_v^{(l)} e^{ih_v^{(l)} \{x+ld_\Delta\}}] \sum_{n=-N}^N u_{v,n}^{(l)} e^{i \frac{2n\pi z}{p}}; \quad l = \frac{M+1}{2}. \quad (11)$$

Then, $A_{v \neq 1}^{(l \neq (M+1)/2)}$ and $B_v^{(l \neq (M+1)/2)}$ of the unknown coefficient for the electromagnetic fields can be founded by solving the simultaneous equation at the center layer of the middle layer. In the case of another layer for the middle layer, unknown coefficients of the electromagnetic fields can be obtained by using the boundary conditions. Similarly, in the case of upper region ($-2d < x < 0$), it is obtained from Eq.(7). In the case of lower region ($-D < x < -3d$), electromagnetic fields can be used to those of the upper region from the symmetric structure. To obtain the distribution of energy flow, the electric fields founded from Eq.(5) are given by

$$E_x^{(2,l)} = \frac{e^{i\gamma z}}{\omega \mathcal{E}(z)} \sum_{v=1}^{2N+1} [A_v^{(l)} e^{-ih_v^{(l)} \{x+(l-1)d_\Delta\}} + B_v^{(l)} e^{ih_v^{(l)} \{x+ld_\Delta\}}] \sum_{n=-N}^N u_{v,n}^{(l)} (\gamma + 2n\pi/p) e^{i \frac{2n\pi z}{p}}, \quad (12)$$

$$E_z^{(2,l)} = \frac{e^{i\gamma z}}{\omega \mathcal{E}(z)} \sum_{v=1}^{2N+1} h_v^{(l)} [A_v^{(l)} e^{-ih_v^{(l)} \{x+(l-1)d_\Delta\}} - B_v^{(l)} e^{ih_v^{(l)} \{x+ld_\Delta\}}] \sum_{n=-N}^N u_{v,n}^{(l)} e^{i \frac{2n\pi z}{p}}. \quad (13)$$

Therefore, using the Eqs.(12) and (13), x - and z -components of Poynting vector are given by following equations for TM mode:

$$S_x^{(TM)} \triangleq \text{Re} [E_z^{(2,l)} \times (H_y^{(2,l)})^*] / 2, \quad S_z^{(TM)} \triangleq \text{Re} [E_x^{(2,l)} \times (H_y^{(2,l)})^*] / 2, \quad (14)$$

The distribution of energy flow in the numerical analysis are given by

$$P^{(TM)} \triangleq \sqrt{\{S_x^{(TM)}\}^2 + \{S_z^{(TM)}\}^2}. \quad (15)$$

3. Numerical Results

We consider the lowest guided TM_0 and TE_0 modes ($0 < p/\lambda < 0.5$), and the structure based on the circular cylinders ($c/p = b/p = 1/6$) as rhombic dielectric structure in the middle layer. The values of parameters chosen are $\epsilon_a/\epsilon_0 = 3$, $\epsilon_b/\epsilon_0 = 3$, $\epsilon_3/\epsilon_0 = 3$, $d_1/d = 1$, $D/p = 5/6$, $2a/d_1 = 1$, $c/p = 1/6$, $b/p = 1/6$. The numerical computation in this paper is performed using the parameter $N=10$ or $N=9$ for TE and TM modes and $M=40$ which make the relative error to the extrapolated true values less than about 1%. We use the excited normalized frequency p/λ at the guided area of $\epsilon_3^{(m)}/\epsilon_0 = 3$ with the stop band region of $\epsilon_3^{(m)}/\epsilon_0 = 1$ as shown in Figs.2 and 3.

Figures 2(a) and 2(b) show the distribution of the energy flow $P^{(TM)}$ at the guided area for the case of loaded with dielectric triangular cylinder as excited normalized frequency $p/\lambda = 0.455$ and rhombic dielectric structure as excited normalized frequency $p/\lambda = 0.454$ in the middle layer as a condition of $\epsilon_3^{(m)}/\epsilon_0 = 3$ for TM_0 mode, respectively. From these figures, we can see the following features:

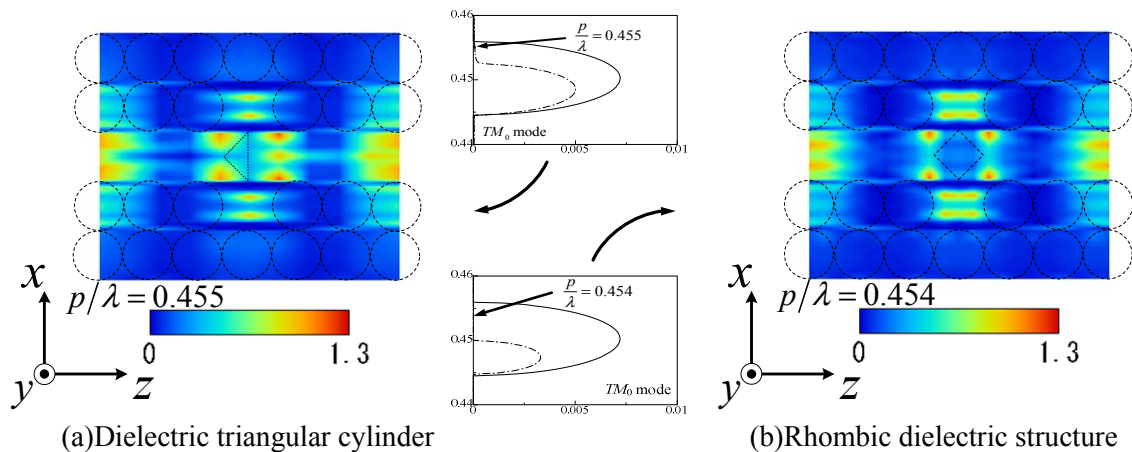
- (1) The energy of defect area for rhombic dielectric structure is stronger than that of dielectric triangular cylinder.
- (2) The middle layer region loaded with the rhombic dielectric structure instead of dielectric triangular cylinder can be obtained distribution of symmetry.

Figures 3(a) and 3(b) show the distribution of energy flow $P^{(TE)}$ at the guided area for the case of loaded with dielectric circular cylinders as excited normalized frequency $p/\lambda = 0.405$ and rhombic dielectric structure as $p/\lambda = 0.407$ in the middle layer as same condition of Fig.2 for TE_0 mode, respectively. From these figures, we can see the following features:

- (1) The energy of defect area for dielectric circular cylinder is strong compared with rhombic dielectric structure.
- (2) In the outside region of the defect area, the distribution of energy flow is similar to the case of dielectric circular cylinder.

4. Conclusions

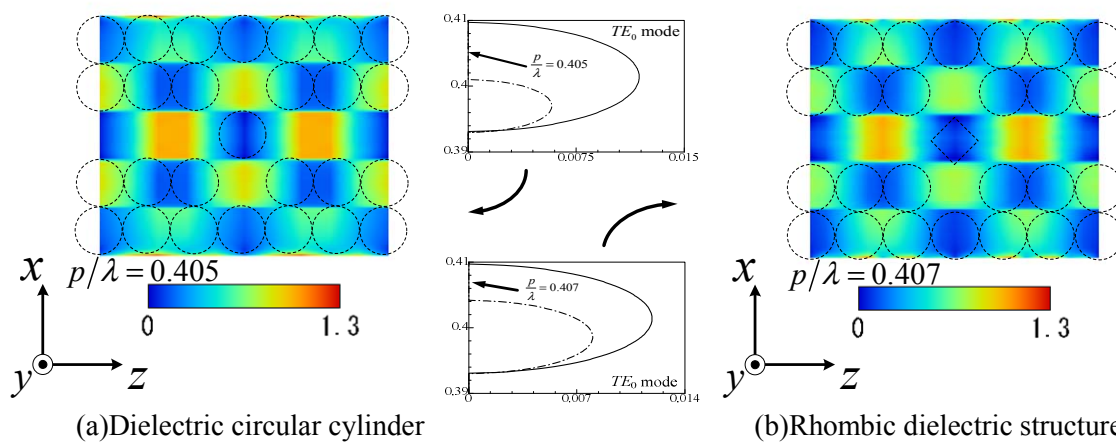
In this paper, we analyzed the guiding problem for dielectric waveguide introduced as defect layers composed of dielectric circular cylinder with symmetric structure such as rhombic dielectric structure along a middle layer, and investigated the distribution of energy flow for dielectric waveguides for both TM_0 and TE_0 modes by using the propagation constants at the guided area.



(a)Dielectric triangular cylinder

(b)Rhombic dielectric structure

Fig.2 Distribution of energy flow $P^{(TM)}$ at the guided area for TM_0 mode



(a)Dielectric circular cylinder

(b)Rhombic dielectric structure

Fig.3 Distribution of energy flow $P^{(TE)}$ at the guided area for TE_0 mode

Numerical results are given for the influence of the middle layer loaded with rhombic dielectric structure in terms of the distribution of energy flow. As numerical results, we can be obtained the confinement efficiency loaded with rhombic dielectric structure compared with dielectric triangular cylinder for TM_0 mode. In the case of TE_0 mode, it is shown obviously that we can be obtained the confinement efficiency loaded with dielectric circular cylinder compared with rhombic dielectric structure. In the future, we will be investigated the influence of convergence for large periodic length and optimum shape in the middle layer.

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