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RESONANT FREQUENCY OF EQUILATERAL TRIANGULAR PATCH RESONATOR WITH SUPERSTRATE USING MODIFIED WOLFF MODEL

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ABSTRACT:

A new model called modified Wolff model [MWM] recently developed has been used to calculate the resonant frequency of various modes of the equilateral triangular patch within 0.5% of reported experimental results. MWM also accounts for the effect of dielectric superstrate on the resonant frequency. MWM has already been used to calculate the resonant frequency of covered rectangular and circular patches within 0.5% accuracy. Thus MWM is suitable for microwave CAD.

INTRODUCTION

The triangular patch resonator is an attractive microstrip element useful for the design of compact and broader bandwidth circulator, filter and oscillator. As a radiating element it has wide half-power beamwidth in both E&H planes and has no null in the endfire direction. The cavity model has been used by several authors [1-3] to calculate resonant frequency of various modes. Dahele and Lee [1] have presented experimental results on the resonant frequency of five modes and improved the cavity model by replacing side length of equilateral triangle by increased effective sidelength to account for the fringe field. However, they have not replaced ϵ_r of the substrate by ϵ_{eff} to take care of inhomogeneity of the medium. Garg and Long [2] have treated side of equilateral triangle as radius of a circle and obtained more accurate results on the resonant frequency. They have also maintained ϵ_r in the expression for the resonant frequency. Gang [3] has shown that maintaining ϵ_r is not always right. Such assumption is valid for small h/L ratio. Moreover, the cavity model in its standard form is not suitable for calculation of resonant frequency with superstrate. Fullwave analysis results for equilateral triangular patch with and without cover are not available. Recently authors have developed a modified Wolff model [MWM] to calculate the resonant frequency of the covered rectangular [4] and circular patches [5] with accuracy of 0.5% compared to experimental and SDA results. In this paper we have applied MWM to calculate the resonant frequency of the covered equilateral triangular patch shown in fig.(1a).

MODEL

Resonant frequency of the covered patch could be obtained from [3]

$$f_{m,n,l} = \frac{2V_0}{3L_{\text{eff}} (\epsilon_{\text{dyn}})^{1/2}} (m^2 + mn + n^2)^{1/2} \quad (1)$$

where V_0 is velocity of light and the modal integers m, n, l satisfy the condition $m+n+l=0$. L_{eff} is the extended side of the triangular patch due to the fringe field. $\epsilon_{\text{dyn}} (\epsilon_{r1}, \epsilon_{r2}, W, h_1, h_2)$ is the dynamic dielectric constant of the patch with superstrate obtained from

$$\epsilon_{\text{dyn}} (\epsilon_{r1}, \epsilon_{r2}, W, h_1, h_2) = \frac{\epsilon_{\text{dyn}} (\epsilon_{r1}, \epsilon_{r2}, w, h_1, h_2)}{\epsilon_{\text{dyn}} (\epsilon_{r1} = \epsilon_{r2} = 1, W, h_1, h_2)} \quad (2)$$

To calculate L_{eff} and ϵ_{dyn} the equilateral triangular patch has been reduced to an equivalent rectangular patch without changing the length of triangle, fig.(1b). Width W of the equivalent rectangular patch is $0.433L$.

$$C_{\text{dyn}} = \frac{C_{o,\text{stat}}}{\gamma_n \gamma_m} + \frac{C_{,\text{stat}}}{\gamma_n} \quad (3)$$

$$\gamma_i = \begin{cases} 1 & i=0 \\ 2 & i \neq 0 \end{cases} \quad i = n, m \quad (4)$$

where, the first term of equation (3) is dynamic central capacitance of the patch which is not influenced by the superstrate. Therefore,

$$C_{o,\text{stat}} = \frac{\epsilon_{r0} \epsilon_{r1} A}{h} \quad (5)$$

where, A is the area of the equilateral triangle. The fringe capacitance along the length L is obtained from

$$C_{e,\text{stat}} = \frac{1}{2} \left[\frac{Z(W, h_1, h_2, \epsilon_{r1}, \epsilon_{r2} = 1) XL}{v_0 Z^2(W, h_1, h_2, \epsilon_{r1}, \epsilon_{r2})} - C_{o,\text{stat}} \right] \quad (6)$$

where Z is the characteristic impedance of the line. The effective length L_{eff} of the covered patch can be obtained from Long and Garg formula which has been adopted for covered patch also [4].

RESULTS

The calculated resonant frequency of the $L=10\text{cm}$ equilateral patch on substrate $\epsilon_{r1}=2.32$, $h_1=0.159\text{ cm}$ is shown in the table-1 along with measured resonant frequency and resonant frequency calculated by Garg-Long [2] Dahele-Lee[1], and Gang[3]. Gang attempted to rationalize the calculation of resonant frequency of triangular patch.

However, his method gives maximum average error i.e. 1.9% compared to the experimental values. MWM provides average error 0.26% and error remains always within 0.5%. The method adopted by Garg and Long also gives good result but is applicable to the single layer structure only. Effect of the cover on various modes of the triangular Patch is shown in fig.(2)

CONCLUSION

The MWM can be effectively used to calculate resonant frequency of the multilayered rectangular, circular and equilateral triangular patches with the accuracy of fullwave analysis while retaining advantages of cavity model. The method is suitable for microwave CAD.

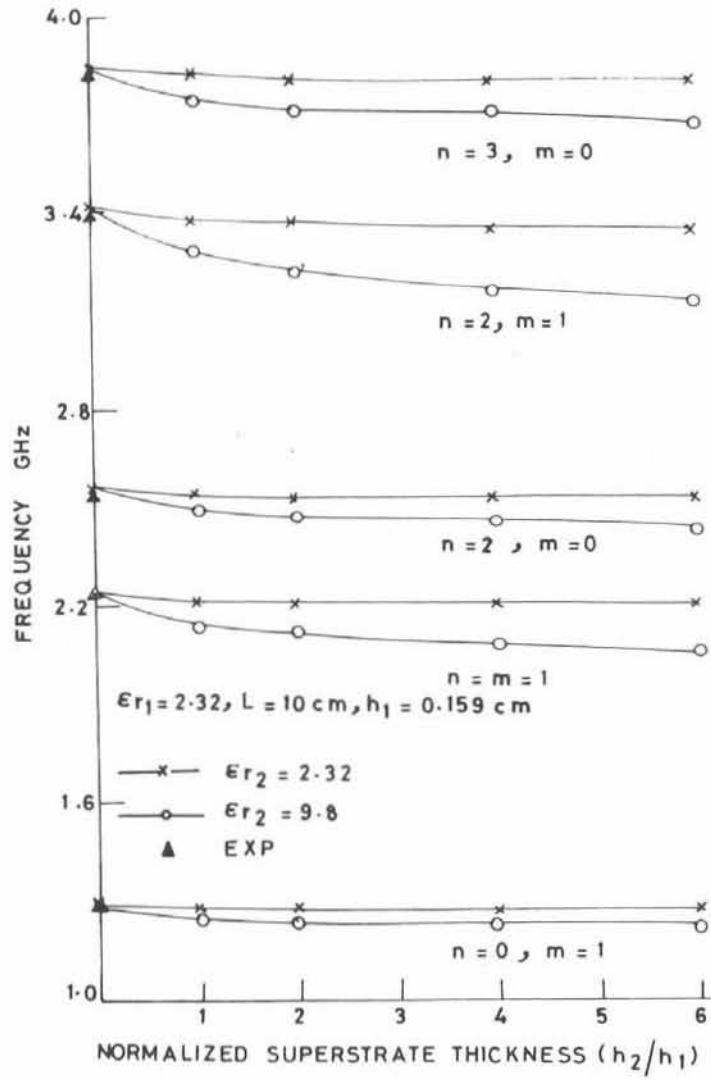
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Table 1

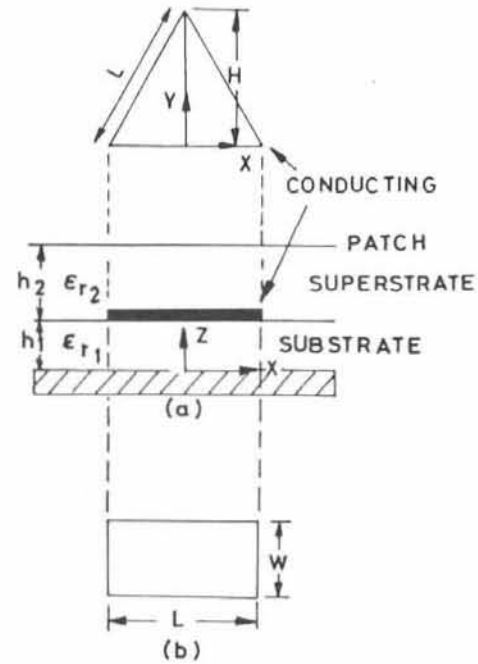
Resonant Frequency of Equilateral Triangular Patch by various methods.

TM	fr exp GHz	Garg fr [3] GHz	Error %	Dahele fr [1] GHz	Error %	Garg fr[2] GHz	Error %	MWM fr GHz	Error %
10	1.280	1.306	2.03	1.299	1.8	1.273	0.5	1.280	0.0
11	2.242	2.262	0.89	2.252	1.45	2.239	0.1	2.239	0.1
20	2.550	2.612	2.40	2.599	1.92	2.546	0.3	2.560	0.3
21	3.400	3.456	1.65	3.439	1.15	3.419	0.5	3.420	0.5
30	3.824	3.919	2.48	3.899	1.96	3.81	0.1	3.840	0.4



EFFECT OF SUPERSTRATE ON F_r

FIG-2



(a) : EQUILATERAL TRIANGULAR PATCH RESONATOR WITH SUPERSTRATE

(b) : EQUIVALENT RECTANGULAR PATCH

FIG . 1