

Convenient Co-channel Interference Detection Methods for Digital Cellular Radio

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1. INTRODUCTION

In a cellular or microcellular system, the signal transmission performance is generally limited not by additive thermal noise but by co-channel interference [1]. Thus, the detection of carrier to co-channel interference ratio (C/I) is of great importance for monitoring the channel quality.

In this paper, we show that the multipath delay spread estimation method previously proposed by the authors [2][3] can be applied to the detection of C/I for BPSK and for $\pi/4$ -shift QPSK [4]. It is possible to estimate C/I using quadrature-channel (Q-ch) detector output for a BPSK signal and using amplitude difference between in-phase channel (I-ch) and Q-ch detector outputs for a $\pi/4$ -shift QPSK signal. The results of computer simulation and laboratory experiment prove that the proposed scheme is very useful for in-service monitoring of C/I .

2. PRINCIPLES

Fig.1 shows a block diagram of a differential detector for BPSK. If the upper part, i.e. I-ch, is assumed to yield a normal eye pattern of a BPSK signal, then the lower part shows the Q-ch detector output and no signal appears generally. However, when an interference signal is added to the original signal, non-zero signal appears even at this Q-ch detector output. We will try to estimate C/I from this Q-ch output.

Fig.2 shows a differential detector for $\pi/4$ -shift QPSK. In this case, obviously the C/I quantity cannot be obtained from the Q-ch detector output directly. We note that, for $\pi/4$ -shift QPSK, generally $|I| = |Q|$ holds true, where $|I|$ and $|Q|$ mean the magnitudes of I-ch and Q-ch outputs, respectively. However, if an interference signal exists, then signal constellation is getting distorted and $|I| = |Q|$

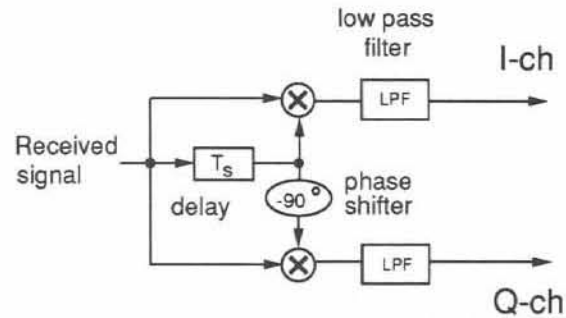


Fig.1 Block diagram of differential detector for BPSK.

does not necessarily holds. Thus, we expect that information on C/I is obtained from the measurement of averaged $||I| - |Q||$.

When only one interference signal exists, the I-ch and Q-ch outputs of a differential detector are calculated for both BPSK and $\pi/4$ -shift QPSK, as follows:

$$I = A_C^2 \{ \cos \Delta\theta_C + \rho \cos(\Delta\theta_C + \phi) + \rho \cos(\Delta\theta_I - \phi) + \rho^2 \cos \Delta\theta_I \}$$

$$Q = A_C^2 \{ \sin \Delta\theta_C + \rho \sin(\Delta\theta_C + \phi) + \rho \sin(\Delta\theta_I - \phi) + \rho^2 \sin \Delta\theta_I \}$$

where ϕ is a phase difference between carrier and interference, A_C is a magnitude of carrier, A_I is a magnitude of interference, and $\rho = A_I/A_C$. $\Delta\theta_C, \Delta\theta_I \in \{0, \pi\}$ for BPSK, and $\Delta\theta_C, \Delta\theta_I \in \{\pm\pi/4, \pm3\pi/4\}$ for $\pi/4$ -shift QPSK are carrier phase shifts of C and I over a symbol period, respectively.

For BPSK, if each of four phases of $\Delta\theta_C$ and $\Delta\theta_I$ takes place equally likely and ϕ is uniformly distributed, then averaged $|Q|$, denoted as $\overline{|Q|}$, is calculated as follows:

$$\overline{|Q|} = \rho A_C^2 K \quad (K \text{ is a constant})$$

For $\pi/4$ -shift QPSK, if $\rho \ll 1$, the polarity of the above Q-ch output expression is determined by the first term. Then the expression

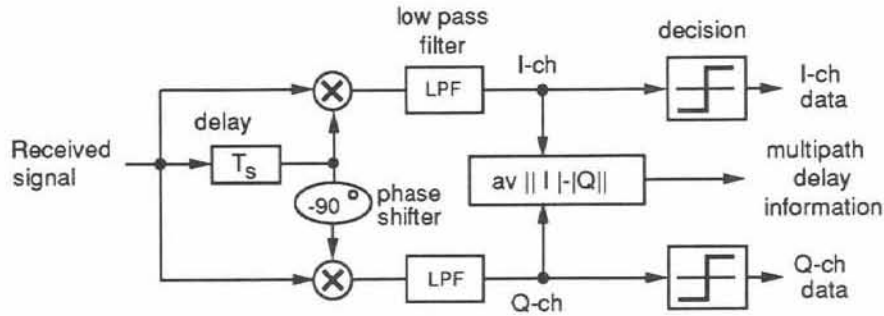


Fig.2 Block diagram of differential detector for $\pi/4$ -shift QPSK.

of $||I| - |Q||$ can be derived assuming that phases $\Delta\theta_C$, and $\Delta\theta_I$ occur with the same probabilities and ϕ is uniformly distributed, i.e.,

$$\overline{||I| - |Q||} = \rho A_C^2 K' \quad (K' \text{ is a constant})$$

To sum up, for both BPSK and $\pi/4$ -shift QPSK, it is possible to detect interference signal level or C/I from the measurement of $\overline{|Q|}$ or $\overline{||I| - |Q||}$. The effect of A_C^2 can be removed by applying the received signal to a hard limiter circuit.

3. COMPUTER SIMULATION

3.1 COMPUTER SIMULATION MODEL

To examine the characteristic of the proposed method, computer simulation has been performed assuming a propagation model where carrier (C) and interference (I) are subjected to mutually independent Rayleigh fading. A root-Nyquist filter with a roll-off factor of 50% is adopted. We also assumed a hard-limiter in the receiver to avoid the fluctuation of detector output caused by the received signal power variation.

3.2 COMPUTER SIMULATION RESULTS

Fig. 3 shows the simulation result of Q-ch detector output of BPSK plotted against C/I . We observe that $\overline{|Q|}$ increases almost linearly as C/I (dB) decreases from 30 dB to 0 dB when E_b/N_0 is greater than or equal to 30 dB.

For $\pi/4$ -shift QPSK, however, there arises a problem. Due to the transient response caused by a bandwidth restriction filter, $\overline{||I| - |Q||}$ has an offset and its dynamic range shrinks even if C/I changes largely.

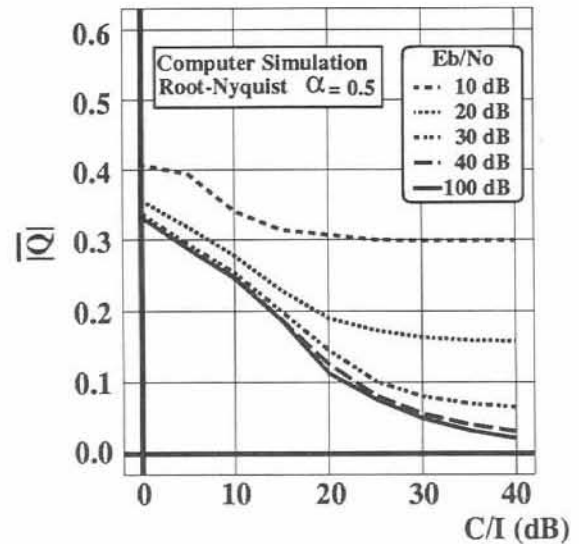


Fig.3 $\overline{|Q|}$ vs. C/I for BPSK.

To avoid this offset, we propose a method that makes use of sampled values of $||I| - |Q||$ at the center of each symbol interval. By applying this sampling method, dynamic range of the output was found to be enlarged. Fig. 4 shows detector output vs. C/I that is obtained by this method. As the curves show, a detector output has a good correspondence with C/I variation.

4. LABORATORY EXPERIMENT

4.1 LABORATORY EXPERIMENT SYSTEM

To confirm the computer simulation result, we made laboratory measurements for $\pi/4$ -shift QPSK. For this purpose, we utilized the same hardware circuit as was used for a multipath delay spread detection [3] shown in Fig. 5.

I-ch and Q-ch detector outputs are sampled

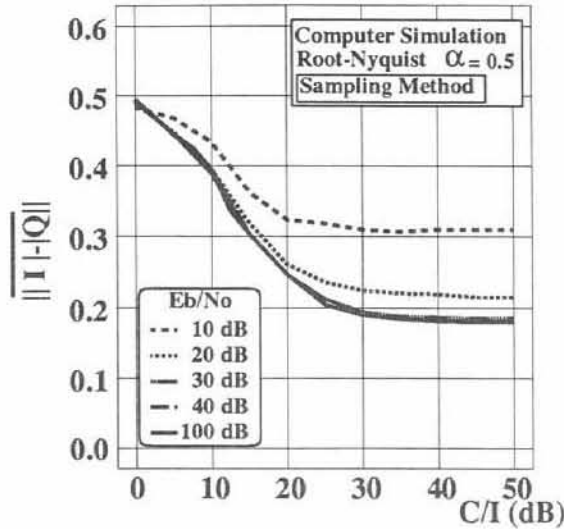


Fig.4 $\frac{||I| - |Q||}{C/I}$ vs. C/I for $\pi/4$ -shift QPSK.

by the recovered clock, and then quantized by 8bit A/D converter. $||I| - |Q||$ is calculated and accumulated to give an averaged $||I| - |Q||$ by a digital circuit.

Fig. 6 shows a block diagram of the laboratory transmission experiment system.

4.2 EXPERIMENTAL RESULTS

First, when only a co-channel interference exists, we found that there existed a good correspondence between C/I and detector output ($||I| - |Q||$). This corresponds to the curve denoted as $\tau/T_S = 0.0$ in Fig. 7.

Next, the monitoring characteristics in a general propagation environment, where both multipath delay spread and co-channel interference exist, are investigated. Fig. 7 shows experimental results showing how detector output vs. C/I relation changes when τ/T_S is increased, assuming a mutually-uncorrelated Rayleigh-distributed two-ray model with average $D/U = 0$ dB and a roll-off filter of $BT_S = 2.0$. When τ/T_S approaches unity, i.e. a very bad condition, detector output is observed to be nearly saturated and is affected only slightly by C/I variation.

As BER was measured at the same time, we plotted the relation between detector output and BER in Fig. 8. In spite of the fact that plotted data in Fig. 8 covers broad range of parameters of laboratory measurement system, i.e., C/I from 0 to 40 dB, τ/T_S from 0 to 1.0 and average D/U from 0 to 12 dB, quite a good relation between BER and detector output was found to our surprise. Therefore, it seems to be possible to estimate to a certain degree of accuracy BER of system from the value of detector output since the scattering

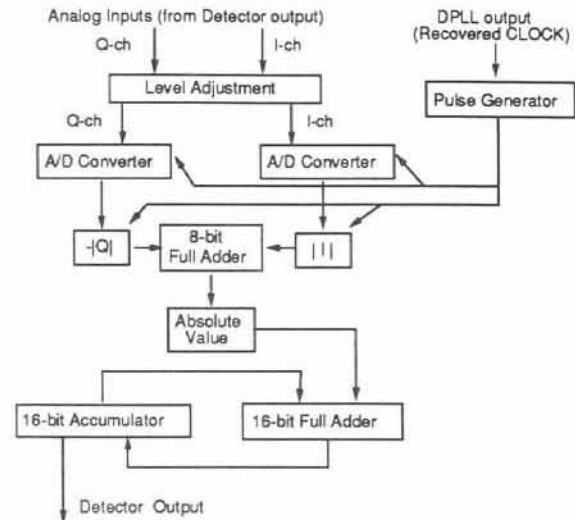


Fig.5 Block diagram of hardware for $||I| - |Q||$ measurement.

of the curves for the various values of parameters is very small.

5. CONCLUDING REMARKS

The relationships between C/I and the value of $|Q|$ for BPSK or $||I| - |Q||$ for $\pi/4$ -shift QPSK were studied by computer simulation and the latter also by laboratory experiments. As a result, it is confirmed that the values of $|Q|$ and $||I| - |Q||$ can be used for in-service monitoring of C/I . To avoid the degradation due to bandwidth restriction for $\pi/4$ -shift QPSK, we proposed the method that measures sampled $||I| - |Q||$.

When multipath delay spread is not negligible, however, the curves $|Q|$ or $||I| - |Q||$ vs. C/I are influenced to a large extent. Even in such a circumstance, we found that quite good relations are observed between BER and $|Q|$ or $||I| - |Q||$. These are very useful relations for in-service monitoring of a channel quality.

Since the C/I is a very important factor in determining the performance of a cellular radio system, the proposed scheme might find a place in various applications for performance improvement, such as in antenna branch selection of the various diversity reception system, and also in decision making of intra- or inter-cell handoff.

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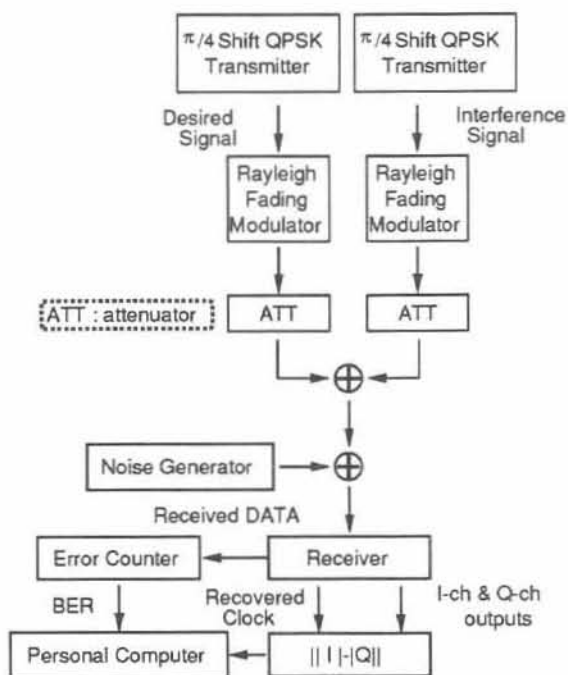


Fig.6 Block diagram of laboratory experiment system.

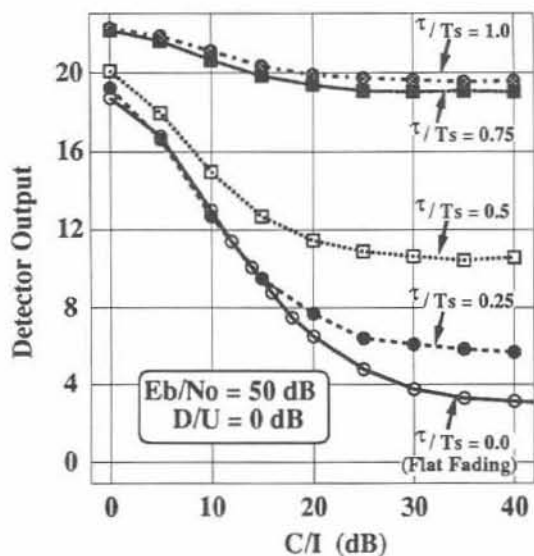


Fig.7 Laboratory measurement of detector output vs. C/I .

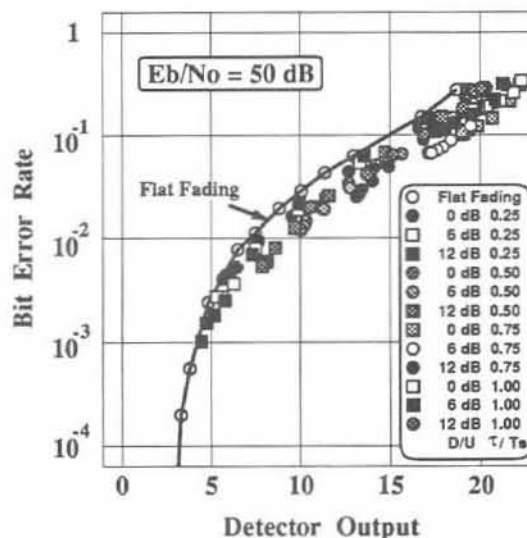


Fig.8 BER vs. detector output (sampling method).

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